

$$2.3) Z(d) = Z_0 \frac{Z_L + j Z_0 \tan \beta d}{Z_0 + j Z_L \tan \beta d}$$

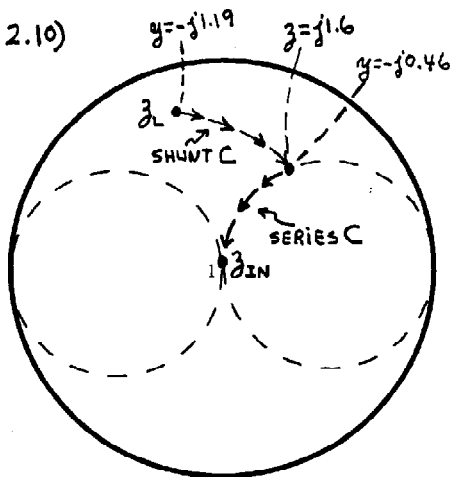
$$Z(d + \frac{n\lambda}{2}) = Z_0 \frac{Z_L + j Z_0 \tan(\beta d + \frac{n\beta\lambda}{2})}{Z_0 + j Z_L \tan(\beta d + \frac{n\beta\lambda}{2})} ; n\beta\frac{\lambda}{2} = \frac{n2\pi\lambda}{\lambda} \frac{\lambda}{2} = n\pi$$

$$\tan(\beta d + n\pi) = \tan \beta d$$

Hence,

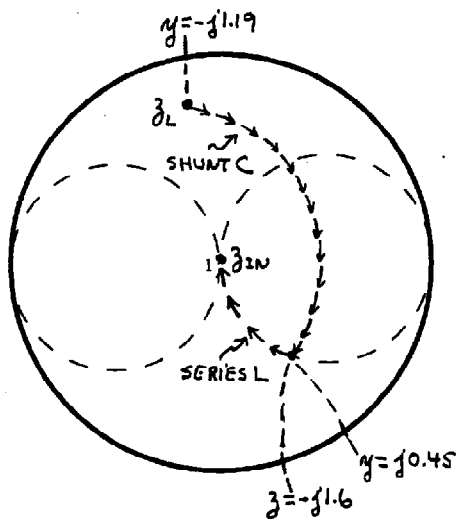
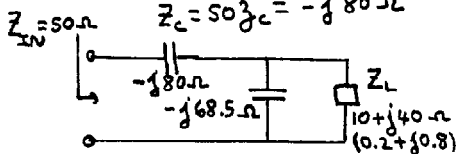
$$Z(d + \frac{n\lambda}{2}) = Z(d)$$

2.10)



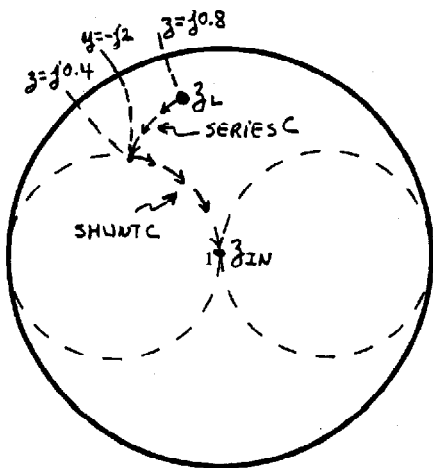
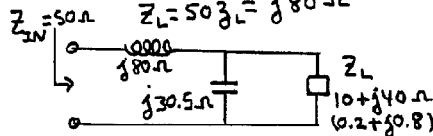
SHUNT C:  $y_c = -j0.46 - (-j1.19) = j0.73$   
 $Z_c = \frac{50}{y_c} = -j68.5 \Omega$

SERIES C:  $z_c = 0 - j1.6 = -j1.6$   
 $Z_c = 50 z_c = -j80 \Omega$



SHUNT C:  $y_c = j0.45 - (-j1.19) = j1.64$   
 $Z_c = \frac{50}{y_c} = -j30.5 \Omega$

SERIES L:  $z_c = 0 - (-j1.6) = j1.6$   
 $Z_c = 50 z_c = j80 \Omega$

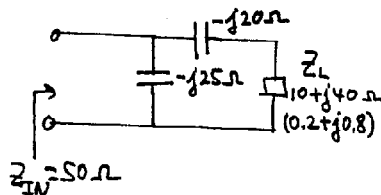


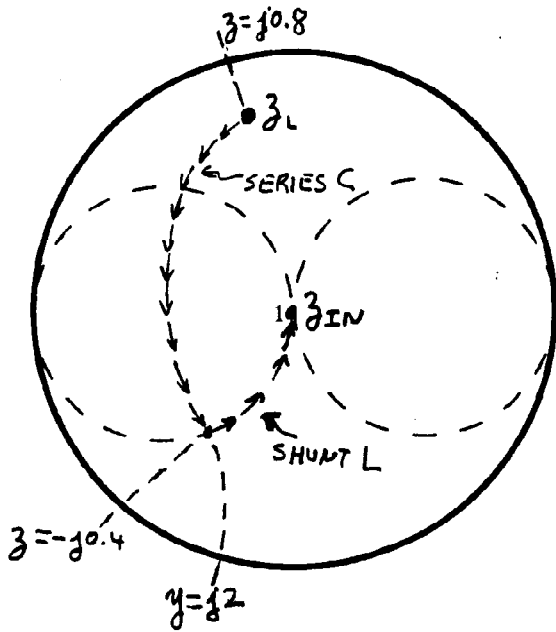
SERIES C:  $z_c = j0.4 - j0.8 = -j0.4$

$$Z_c = 50 z_c = -j20 \Omega$$

SHUNT C:  $y_c = 0 - (-j2) = j2$

$$Z_c = \frac{50}{j2} = -j25 \Omega$$



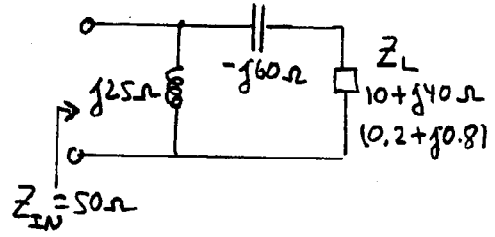


$$\text{SERIES C: } z_c = -j0.4 - j0.8 = -j1.2$$

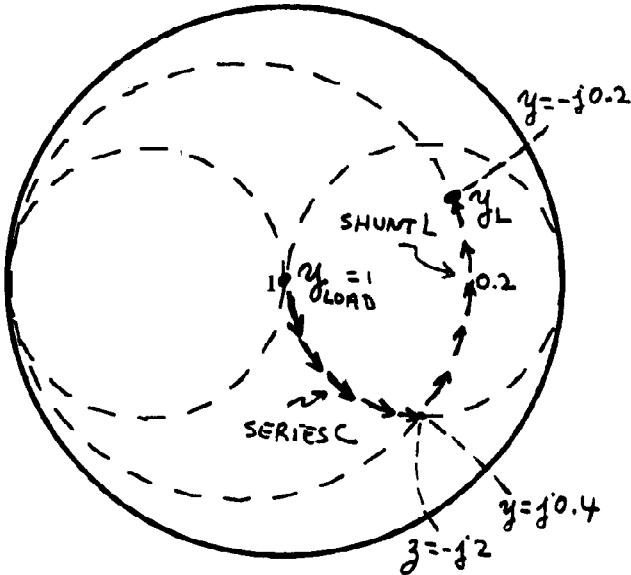
$$Z_c = 50 z_c = -j60 \Omega$$

$$\text{SHUNT L: } y_L = 0 - j2 = -j2$$

$$Z_L = \frac{50}{y_L} = j25 \Omega$$



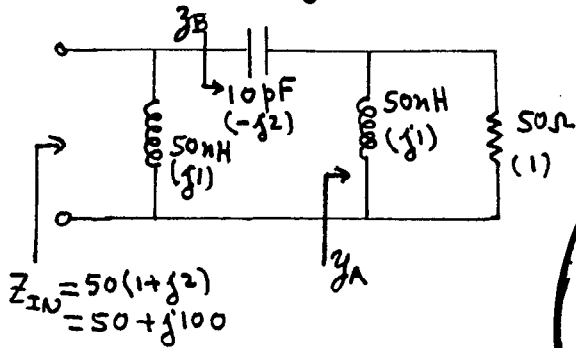
2.11)  $y_L = \frac{Y_L}{Y_0} = Z_0 Y_L = 50(4 - j4)10^{-3} = 0.2 - j0.2$



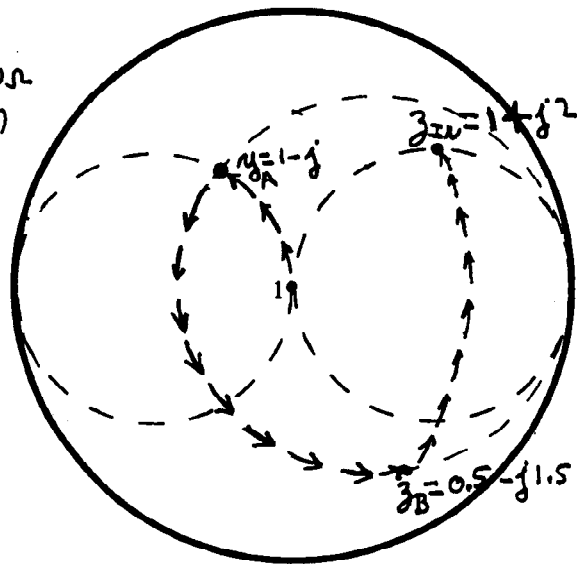
SERIES C:  $z_c = -j2 - j0 = -j2$   
 $Z_c = 50z_c = -j100 \Omega$   
 SHUNT L:  $y_L = -j0.2 - j0.4 = -j0.6$   
 $Z_L = \frac{50}{y_L} = j83.3 \Omega$

AT  $f = 700 \text{ MHz}$ :  
 $Z_L = j\omega L = j83.3$   
 $L = \frac{83.3}{2\pi \cdot 700 \cdot 10^6} = 18.9 \text{ nH}$   
 $Z_c = \frac{-j}{\omega C} = -j100$   
 $C = \frac{1}{100(2\pi \cdot 700 \cdot 10^6)} = 2.27 \text{ pF}$

2.13)  $Z_L = j\omega L = j10^9 \cdot 50 \cdot 10^{-9} = j50$  OR  $z_L = j\frac{50}{50} = j1$   
 $Z_c = \frac{1}{j\omega C} = \frac{1}{j10^9 \cdot 10 \cdot 10^{-12}} = -j100$  OR  $z_c = -j\frac{100}{50} = -j2$



$z_{IN} = 1 + j2$   
 $Z_{IN} = 50z_{IN} = 50 + j100 \Omega$



2.15) (a)  $\beta_L = \frac{50}{50} = 1$

$\beta_{IN} = \frac{20 + j20}{50} = 0.4 + j0.4$

DRAW THE  $Q=5$  CIRCLES (SEE FIG. 2.4.16)

THE MOTION FROM A TO B -- SERIES  $L_1$ :

AT B:  $\beta_B = 1 + j3$

$\beta_{L_1} = j3$  OR  $Z_{L_1} = j3(50) = j150 \Omega$

THE MOTION FROM B TO C -- SHUNT C:

AT B:  $y_B = 0.1 - j0.3$

AT C:  $y_C = 0.1 + j0.5$

$y_C = j0.5 - (-j0.3) = j0.8$

$Z_C = \frac{50}{j0.8} = -j62.5 \Omega$

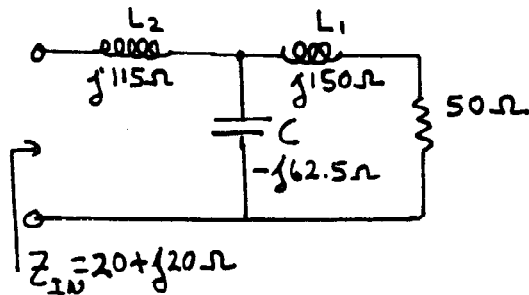
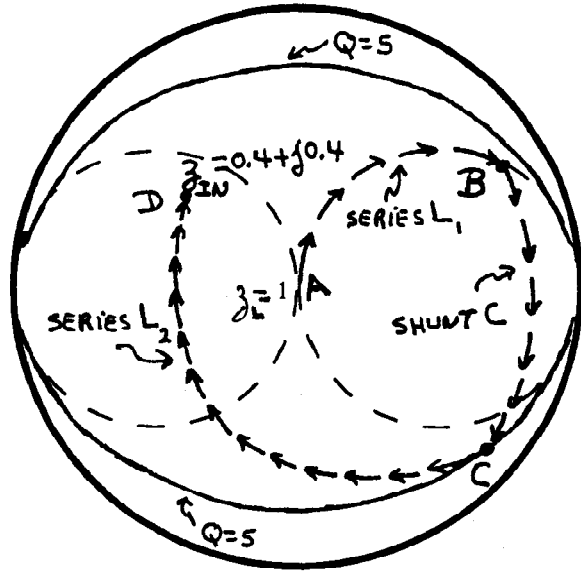
THE MOTION FROM C TO D -- SERIES  $L_2$ :

AT C:  $\beta_C = 0.4 - j1.9$

AT D:  $\beta_D = 0.4 + j0.4$

$\beta_{L_2} = j0.4 - (-j1.9) = j2.3$

$Z_{L_2} = 50(j2.3) = j115 \Omega$



(b)  $\beta_L = 1$  AND  $\beta_{IN} = 0.5$

AT B:  $y_B = 1 - j2.6$ ,  $\beta_B = 0.13 + j0.335$

AT C:  $y_C = 2 - j3.4$ ,  $\beta_C = 0.13 + j0.215$

AT D:  $y_D = 2$ ,  $\beta_D = \beta_{IN} = 0.5$

SHUNT  $L_1$ :  $y_{L_1} = -j2.6$

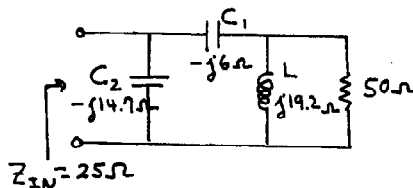
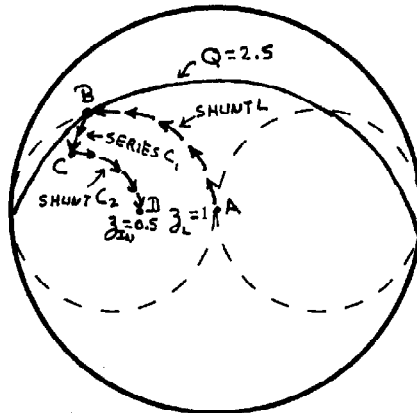
$Z_{L_1} = \frac{50}{-j2.6} = j19.2 \Omega$

SERIES  $C_1$ :  $\beta_C = j0.215 - j0.335 = -j0.12$

$Z_{C_1} = 50(-j0.12) = -j6 \Omega$

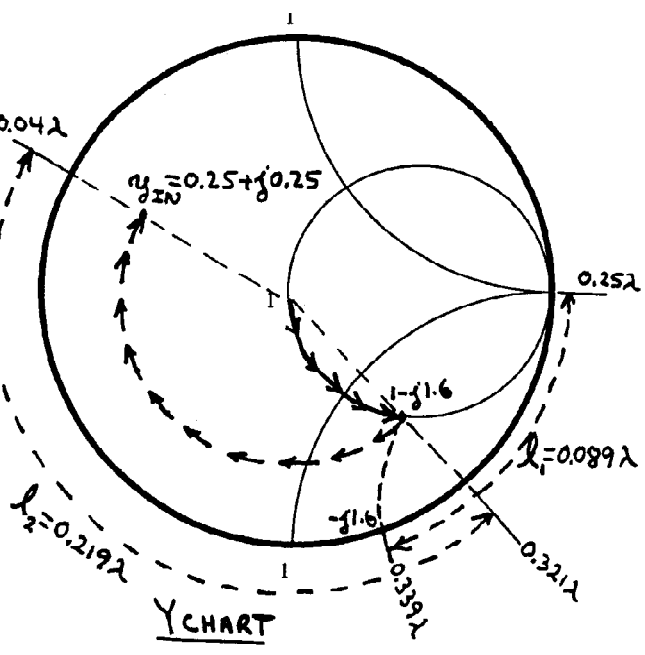
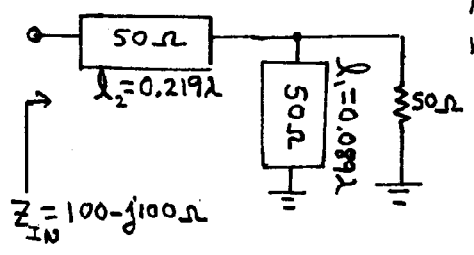
SHUNT  $C_2$ :  $y_{C_2} = 0 - (-j3.4) = j3.4$

$Z_{C_2} = \frac{50}{j3.4} = -j14.7 \Omega$



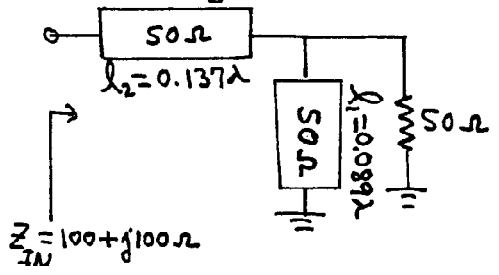
2.19) (a)  $Z_{IN} = \frac{Z_{IN}}{50} = 2 - j2$   
 $y_{IN} = \frac{1}{Z_{IN}} = 0.25 + j0.25$

$l_1 = 0.339\lambda - 0.25\lambda = 0.089\lambda$   
 $l_2 = 0.04\lambda + (0.5\lambda - 0.321\lambda) = 0.219\lambda$

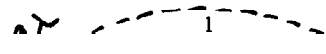


(b) If  $l_1$  is an OPEN-CIRCUITED STUB, THEN  
 $l_1 = 0.25\lambda + 0.089\lambda = 0.339\lambda$

(c) For  $Z_{IN} = \frac{Z_{IN}}{50} = 2 + j2$ , ONE ANSWER IS:



IF  $l_1$  is an OPEN-CIRCUITED STUB, THEN  
 $l_1 = 0.25\lambda + 0.089\lambda = 0.339\lambda$



2.21) (a)  $Y_{IN} = G_{IN} + jB_{IN} = 50 + j40 \text{ mS}$ ,  $R_{IN} = \frac{1}{G_{IN}} = \frac{1}{50 \times 10^{-3}} = 20 \Omega$   
 $Z_{01} = \sqrt{Z_L R_{IN}} = \sqrt{50(20)} = 31.62 \Omega$

IN A SHORT-CIRCUITED  $\frac{3}{8}\lambda$  STUB:  $Y_{sc} = jY_{02}$ . HENCE,  $jY_{02} = jB_{IN} = j40 \text{ mS}$   
 OR  $Y_{02} = 40 \text{ mS}$ ,  $Z_{02} = \frac{1}{Y_{02}} = 25 \Omega$

(b)  $Y_{IN} = G_{IN} - jB_{IN} = 50 - j40 \text{ mS}$ ,  $R_{IN} = \frac{1}{G_{IN}} = 20 \Omega$ .  
 THEN,  $Z_{01} = \sqrt{50(20)} = 31.62 \Omega$ . IN A SHORT-CIRCUITED  $\frac{1}{8}\lambda$  STUB:  
 $Y_{sc} = -jY_{02}$ . HENCE,  $Y_{02} = 40 \text{ mS}$  OR  $Z_{02} = \frac{1}{40 \times 10^{-3}} = 25 \Omega$ .

(c)  $Y_{IN} = G_{IN} + jB_{IN} = 10 + j20 \text{ mS}$ ,  $R_{IN} = \frac{1}{G_{IN}} = \frac{1}{10 \times 10^{-3}} = 100 \Omega$   
 THEN,  $Z_{01} = \sqrt{50(100)} = 70.7 \Omega$ . IN AN OPEN-CIRCUITED  $\frac{1}{8}\lambda$  STUB:  
 $Y_{oc} = jY_{02}$ . HENCE,  $Y_{02} = 20 \text{ mS}$  OR  $Z_{02} = \frac{1}{20 \times 10^{-3}} = 50 \Omega$ .

(d)  $Y_{IN} = 10 - j20 \text{ mS}$ . HENCE:  $Z_{01} = \sqrt{50(100)} = 70.7 \Omega$ .  
 IN AN OPEN-CIRCUITED  $\frac{3}{8}\lambda$  STUB:  $Y_{oc} = -jY_{02}$ . HENCE,  $Z_{02} = \frac{1}{Y_{02}} = \frac{1}{20 \times 10^{-3}} = 50 \Omega$ .

2.22) (a)  $\Gamma_{in} = 0.5 \angle 90^\circ$ ,  $Z_L = 0.6 + j0.8$

$\therefore y_L = \frac{1}{Z_L} = 0.6 - j0.8$

FROM THE SMITH CHART:

$l_1 = 0.136\lambda$ ,  $l_2 = 0.375\lambda - 0.166\lambda = 0.209\lambda$

IN FIG. P.22(b):

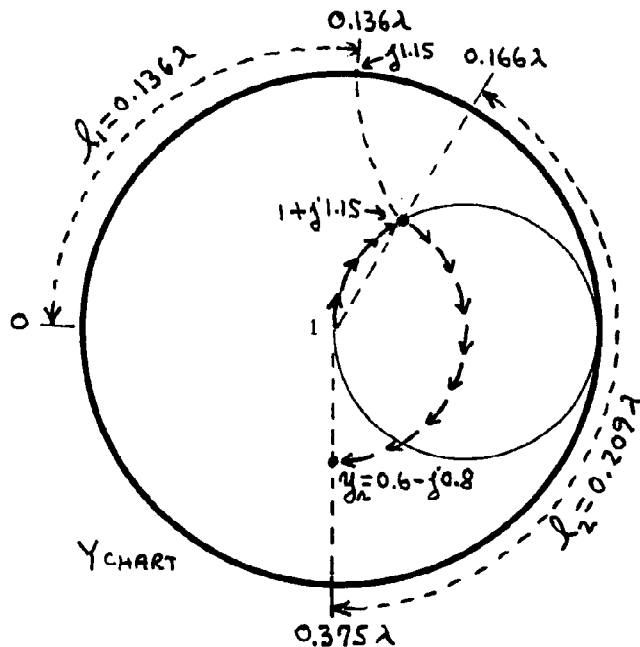
$Y_L = \frac{0.6 - j0.8}{50} = 12 - j16 \text{ mS}$

$\therefore Z_{01} = \sqrt{50 \left( \frac{1}{12 \times 10^{-3}} \right)} = 64.5 \Omega$

USING A  $\frac{3}{8}\lambda$  OPEN-CIRCUITED STUB:

$-jY_{02} = -j16 \text{ mS}$ , OR  $Y_{02} = 16 \text{ mS}$

$Z_{02} = \frac{1}{16 \times 10^{-3}} = 62.5 \Omega$



(b) BALANCED FORM OF THE STUBS.

FOR FIG. P.22(a):  $y_{bal} = j \frac{1.15}{2} = j0.575 \Rightarrow l_{1(bal)} = 0.083\lambda$

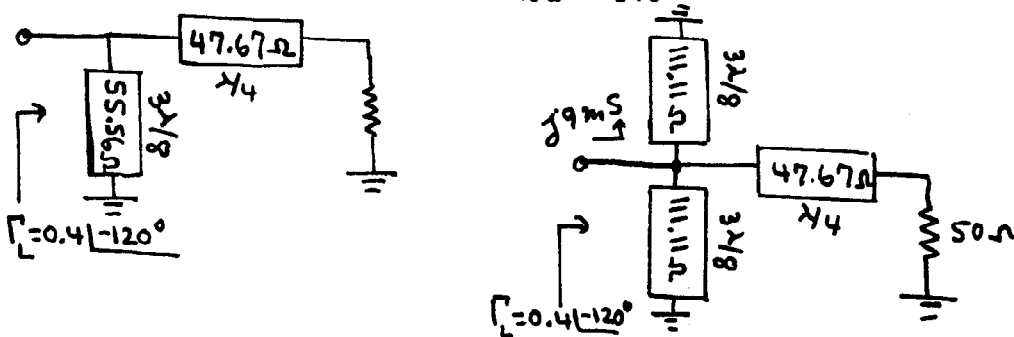
FOR FIG. P.22(b):  $Z_{02(bal)} = 2(62.5) = 125 \Omega$

2.24) (a)  $\Gamma_L = 0.4 \angle -120^\circ$ ,  $Z_L = 0.538 - j0.444$ ,  $y_L = \frac{1}{Z_L} = 1.105 + j0.912$

$Y_L = \frac{y_L}{50} = 22 + j18 \text{ mS}$

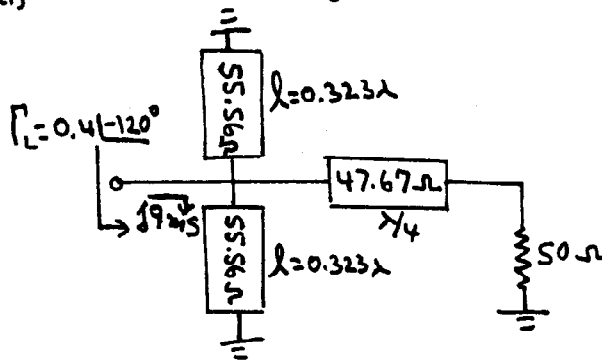
HENCE:  $Z_{o1} = \sqrt{50 \left( \frac{1}{22 \cdot 10^{-3}} \right)} = 47.67 \Omega$  AND

$jY_{o2} = j18 \text{ mS}$  OR  $Z_{o2} = \frac{1}{Y_{o2}} = \frac{1}{18 \cdot 10^{-3}} = 55.56 \Omega$



BALANCE FORM (USE  $2Z_{o2} = 111.11 \Omega$ )

(b) EACH SIDE OF THE BALANCE STUBS HAS AN ADMITTANCE OF  $j9 \text{ mS}$ . IF ITS CHARACTERISTIC IMPEDANCE IS  $Z_0 = \frac{111.11}{2} = 55.56 \Omega$ , THEN  $\gamma_{(bal)} = j9 \cdot 10^{-3} (55.56) = j0.5$ . HENCE:  $l = 0.323 \lambda$ .



2.29)

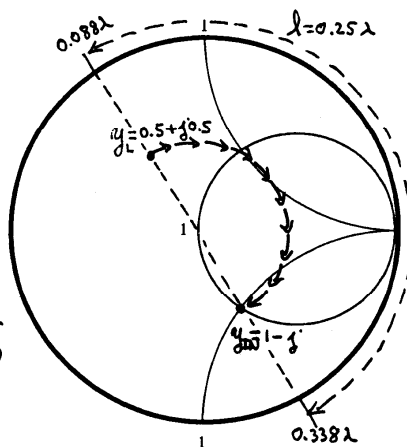
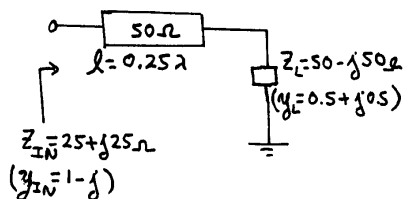
$Z_L = \frac{Z_L}{50} = 1 - j$ ,  $Z_{IN} = \frac{Z_{IN}}{50} = 0.5 + j0.5$

$y_L = \frac{1}{Z_L} = 0.5 + j0.5$ ,  $y_{IN} = \frac{1}{Z_{IN}} = 1 - j$

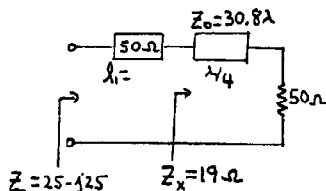
$y_L$  AND  $y_{IN}$  ARE ON THE SAME CONSTANT  $|r|$  CIRCLE. HENCE, A SERIES TRANSMISSION LINE OF LENGTH:

$$l = 0.338\lambda - 0.088\lambda = 0.25\lambda$$

WILL CHANGE  $y_L$  TO  $y_{IN}$ .



2.33) (a)  $Z_{IN} = \frac{25 - j25}{50} = 0.5 - j0.5$

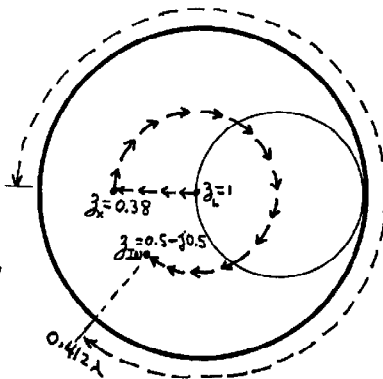


$Z_x$  AND  $Z_{IN}$  MUST BE ON THE SAME CONSTANT  $|r|$  CIRCLE. ONE SOLUTION IS SHOWN ON THE SMITH CHART.

$$Z_x = 50 Z_{IN} = 50(0.38) = 19\Omega$$

THEN:  $Z_0 = \sqrt{Z_L Z_x} = \sqrt{50(19)} = 30.8\Omega$

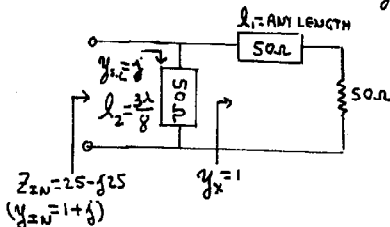
AND  $l_1 = 0.412\lambda$



(b)  $Z_{IN} = 0.5 - j0.5$ ,  $y_{IN} = \frac{1}{Z_{IN}} = 1 + j$

LETTING  $Z_0 = 50\Omega$  AND  $l_1 = \text{ANY LENGTH}$ , THE ADMITTANCE  $y_x = 1$ .

THEN, THE SHUNT STUB MUST PROVIDE:  $y_{s.c} = j$ . HENCE:  $l_2 = \frac{3\lambda}{8}$ .

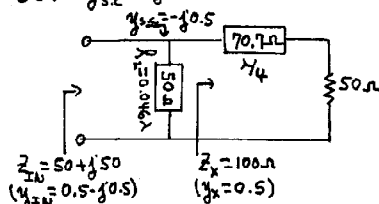


$$y_{IN} = y_x + y_{s.c} = 1 + j$$

(c)  $Z_{IN} = \frac{50 + j50}{50} = 1 + j$ ,  $y_{IN} = 0.5 - j0.5$ ,  $Y_{IN} = 10 - j10 \text{ mS}$

$\therefore Z_0 = \sqrt{Z_L Z_x} = \sqrt{50 \left(\frac{1}{10 \times 10^3}\right)} = 70.7\Omega$ . THE STUB ADMITTANCE MUST

BE:  $y_{s.c} = -j0.5$ . HENCE:  $l_2 = 0.426\lambda$



$$y_{IN} = y_x + y_{s.c} = 0.5 - j0.5$$



2.37) (a) From (2.8.3), with  $\Gamma_L = \Gamma_{IN}^* = 0.545 \angle 77.7^\circ$ , we obtain  $|\Gamma_a| = 0$ .

Then, using (2.8.1),  $(VSWR)_{ch} = 1$ .

(b) When  $\Gamma_L = \Gamma_{IN}^*$  we have  $|\Gamma_a| = 0$  or  $\Gamma_a = 0$ . Hence,

$$Z_a = Z_0 = 50 \Omega$$

$$(c) |\Gamma_a| = \left| \frac{\Gamma_{IN} - \Gamma_L^*}{1 - \Gamma_{IN} \Gamma_L} \right| = \left| \frac{0.4145^\circ - 0.545 \angle -77.7^\circ}{1 - 0.4145^\circ (0.545 \angle 77.7^\circ)} \right| = 0.735$$

$$(VSWR)_{ch} = \frac{1 + 0.735}{1 - 0.735} = 6.54$$