

## Lecture - 4

①

### Matching Networks

A smith chart is the representation in the reflection coefficient plane, called the  $\Gamma$  plane, of the relation

$$\Gamma = \frac{Z - Z_0}{Z + Z_0} \quad - (1)$$

Defining the normalized impedance

$$z = \frac{Z}{Z_0} = \frac{R + jX}{Z_0} = r + jx \quad - (2)$$

We can then rewrite equation 1 as

$$\Gamma = \frac{z - 1}{z + 1}$$

example 1:

Find  $\gamma$  for  $z = 1 + j1$  using the Smith chart (See smith chart)

If the impedance has negative real part we will get a reflection coefficient which will be greater than 1.

If you look at the reflection coefficient line on the Smith chart

example 1

# The Complete Smith Chart

$$y = 0.5 - j0.5$$

Black Magic Design

$$z = 1 + j1$$

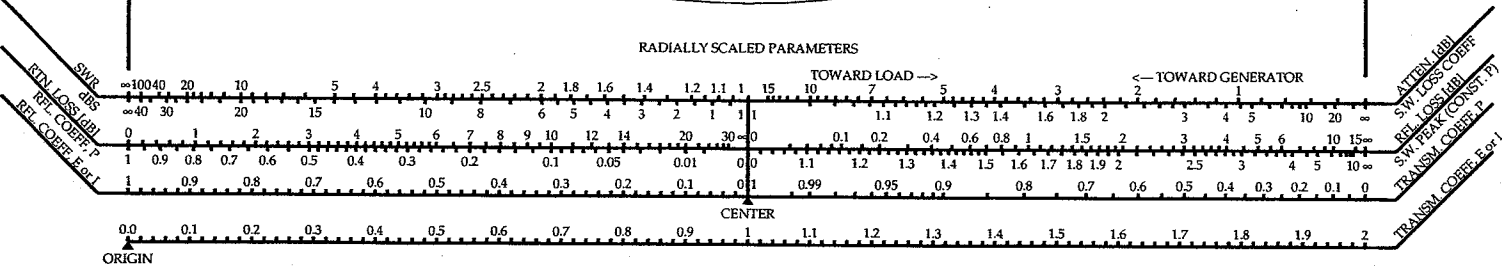
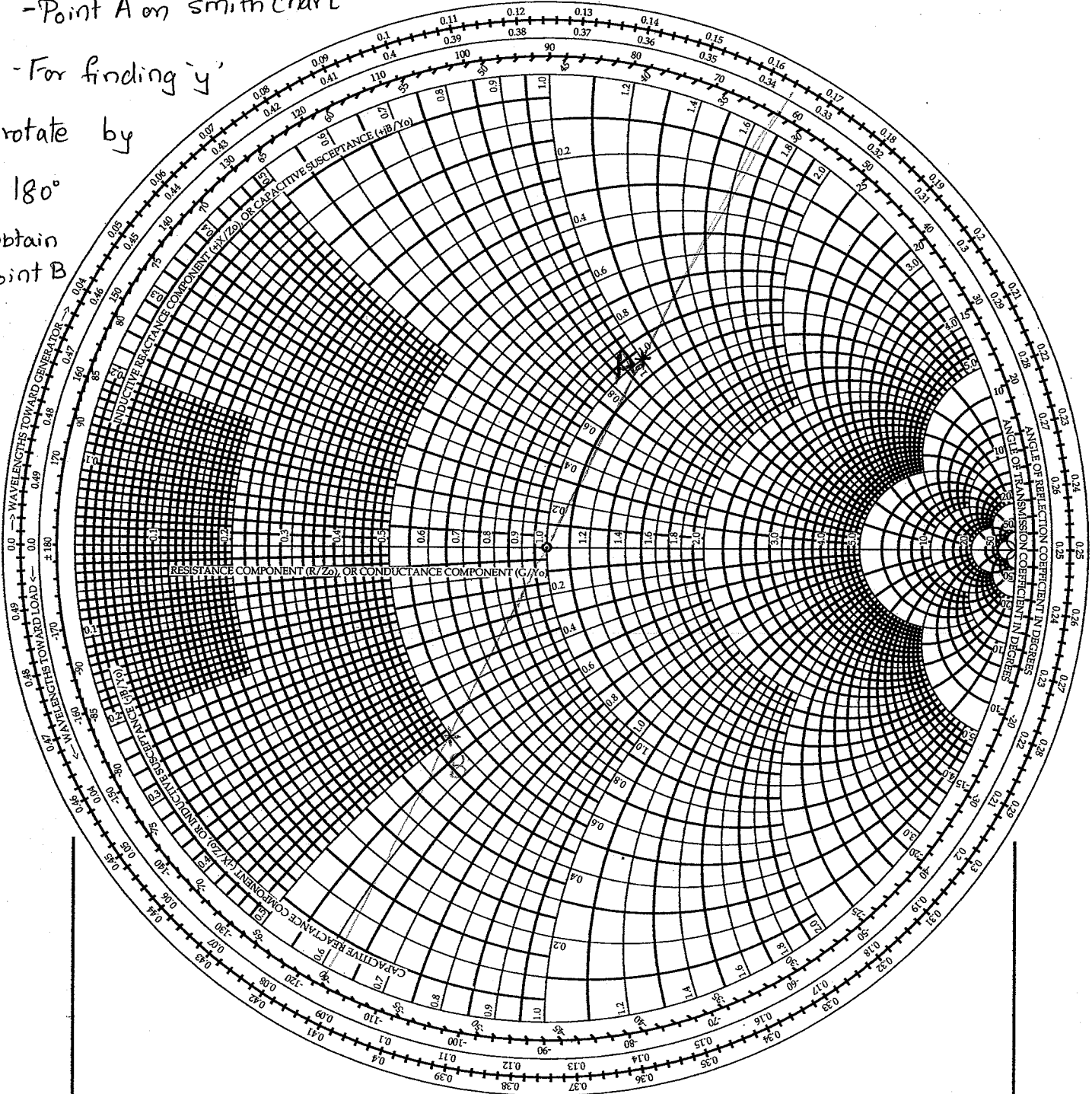
- Point A on smith chart

- For finding 'y'

rotate by

180°

- obtain point B



ATTEN (dB)  
 SWR LOSS COEFF  
 REFL LOSS (dB)  
 SWR PEAK (CONST. P)  
 TRANSM COEFF (P)  
 TRANSM COEFF (E) x 1

you will observe that  $|Γ| > 1$ . For these cases the impedance would map outside the Smith chart. For solving these problems we have to use Compressed Smith chart which looks like the one in Figure 2.2.5. ②

- An alternate way to approach this problem is to plot on the Smith chart  $\frac{1}{Γ}$  and take the values of resistance circles as being negative and the reactance circle as the same as the normal Smith chart.

- Lets do an example

example 2:

Find the impedance whose reflection coefficient is  $2.236 \angle 26.56^\circ$

Soln (See Smith chart)

### Normalized impedance and admittance Smith Chart (ZY Smith chart)

The impedance-to-admittance conversion can also be obtained

by superimposing two Smith charts and rotating one of the charts by  $180^\circ$

The rotated chart represents admittances and the other chart

represents impedances. The superposition of the original and

example 2:

$$\Gamma = 2.236 \angle 26.56^\circ$$

$$\frac{1}{\Gamma^*} = 0.447 \angle 26.56^\circ$$

- Plot this point

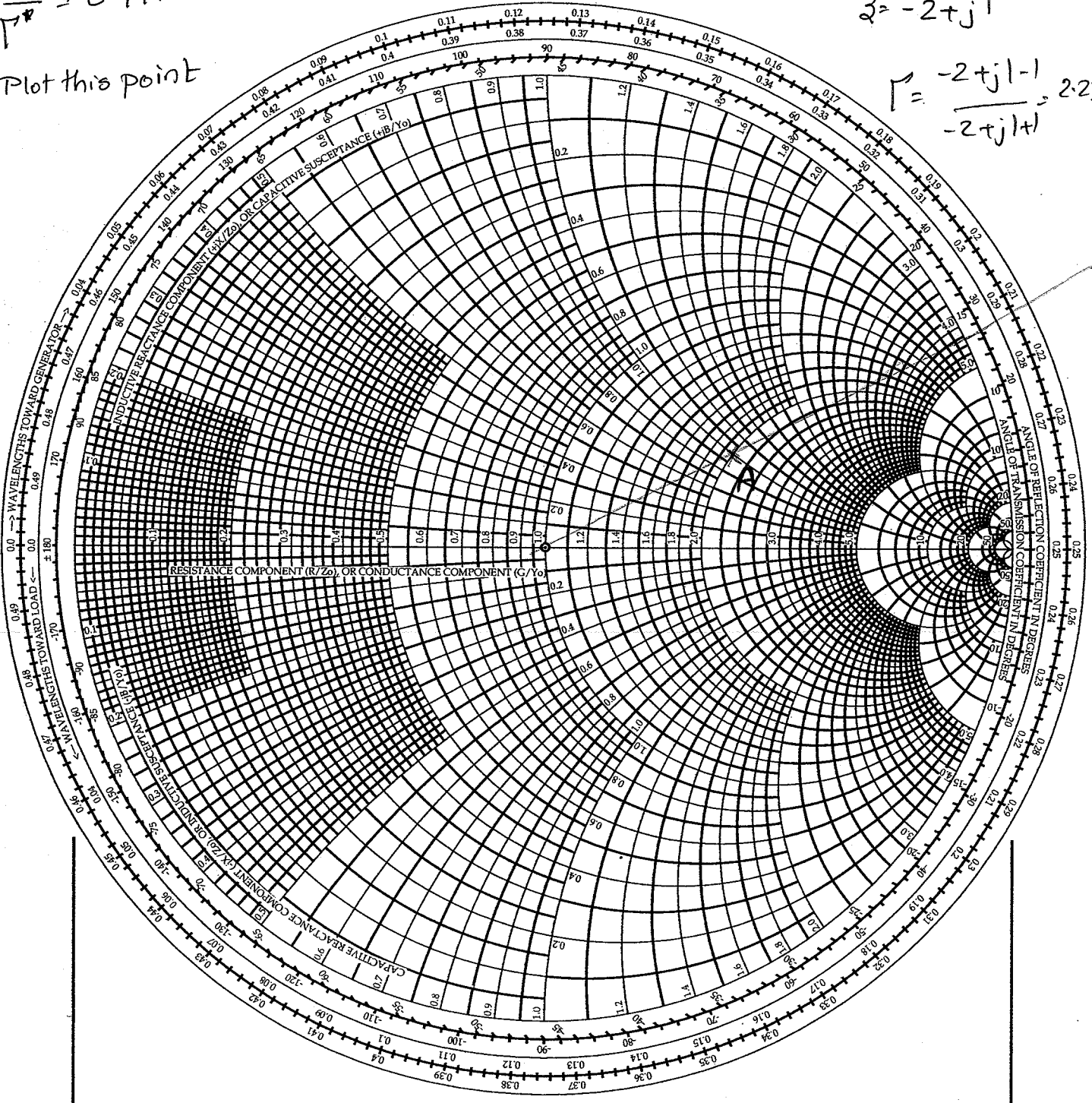
# The Complete Smith Chart

## Black Magic Design

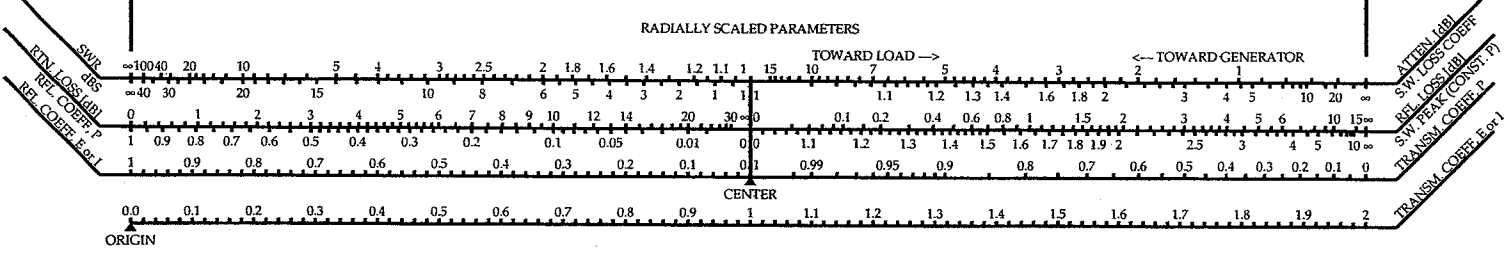
The  $\Gamma$  is then written as

$$\Gamma = -2 + j1$$

$$\Gamma = \frac{-2 + j1}{-2 + j1 + 1} = 2.236 \angle 26.56^\circ$$



### RADIALLY SCALED PARAMETERS



the rotated chart is known as the normalized impedance and admittance coordinates Smith chart. The chart is also referred to as the ZY Smith chart.

- The various Smith charts can be used to represent the frequency response of circuits, or from the frequency response of a circuit in the Smith chart an equivalent circuit model can be developed.
- The simplest frequency responses that can be represented in the Smith chart are those of a series RL circuit, a series RC circuit, a parallel RL circuit, and a parallel RC circuit

Example 3:-

The input equivalent circuit for a transistor on chip is shown in figure below. Determine value of  $R_L$  and  $C$ .

The  $S_{11}$  for this transistor is plotted in figure 1.10.2

Soln

From the figure we observe that

$$f_a = 1 \text{ GHz}$$

$$\begin{aligned} \text{input impedance associated with } S_{11} \text{ is } Z_{IN} &= 50(0.2 - j0.2) \\ &= 10 - j10 \text{ } \Omega \end{aligned}$$

$$z = \frac{Z}{Z_0} = \frac{R + j\omega L}{Z_0} = r + jx$$

Lets assume  $r = 0.2$

and reactance **The Complete Smith Chart (ZY)**

varies from

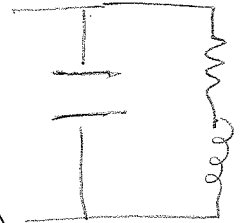
$j0.24$  at  $f_a$  to  $j0.5$  at  $f_b$

If we add capacitor in parallel

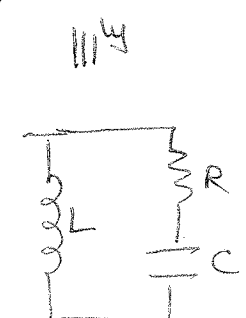
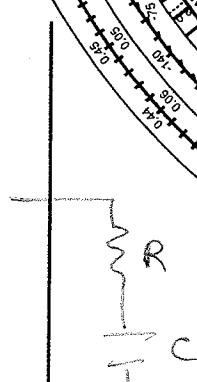
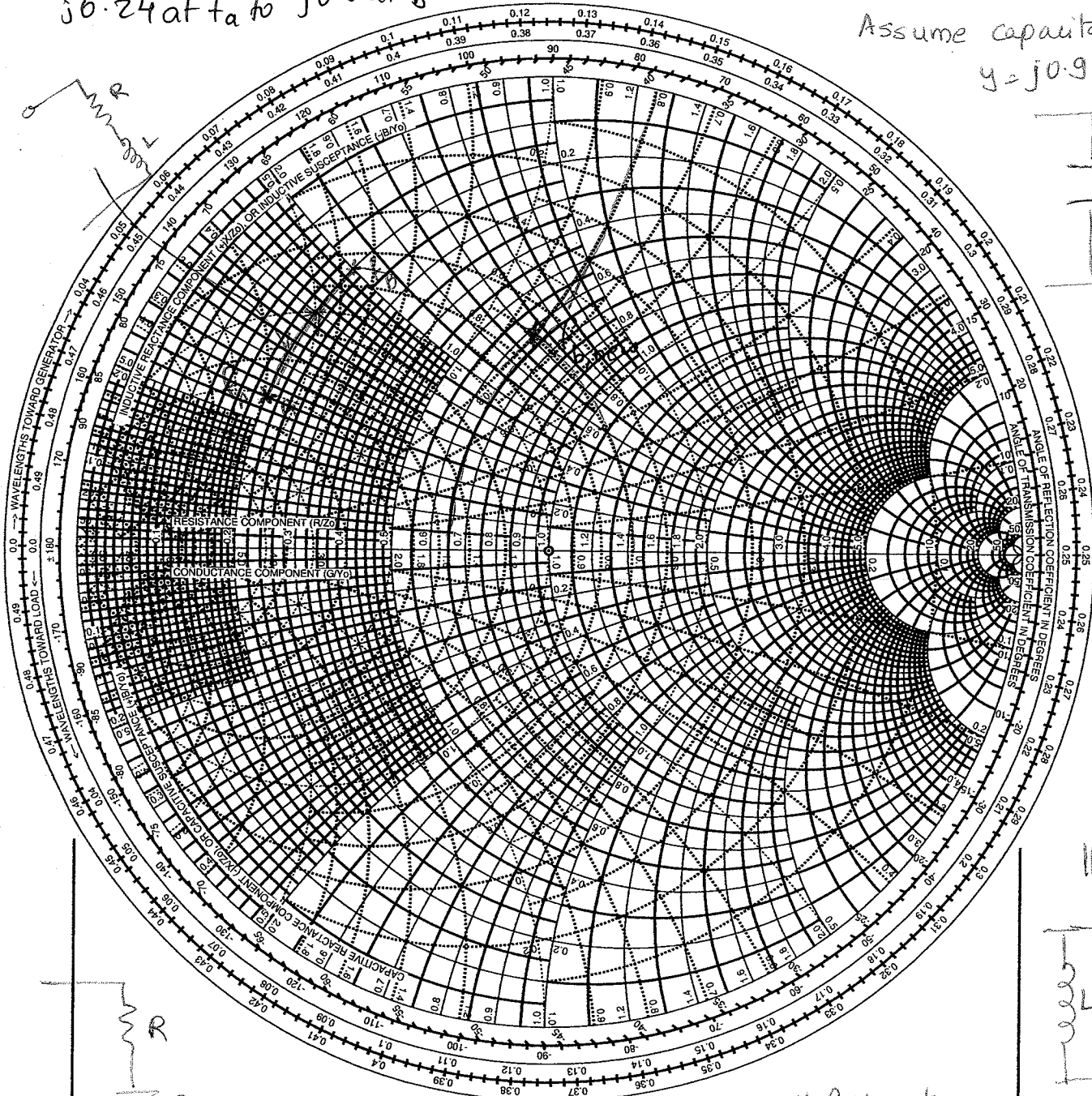
$$z = 0.2 + j0.5$$

$$y = 0.7 - j1.7$$

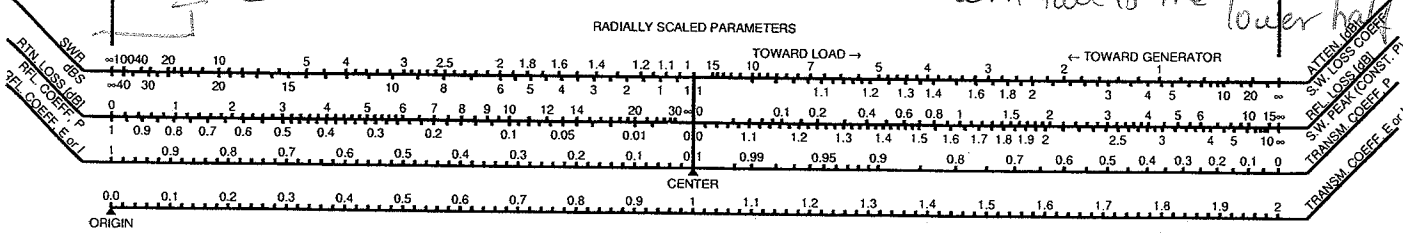
Assume capacitor has  $y = j0.9$



$$y_{f_{new}} = 0.7 - j0.8$$



will fall to the lower half of the Smith Chart



Smith Chart

$$f_b = 10 \text{ GHz} \quad Z_{IN} = 50(0.2 + j0.15) = 10 + j7.5$$

(4)

From the equivalent circuit we have

At  $f_a = 1 \text{ GHz}$

$$10 - j10 = R + j \left[ \omega_a L - \frac{1}{\omega_a C} \right] \quad - (1)$$

At  $f_b = 10 \text{ GHz}$

$$10 + j7.5 = R + j \left[ \omega_b L - \frac{1}{\omega_b C} \right] \quad - (2)$$

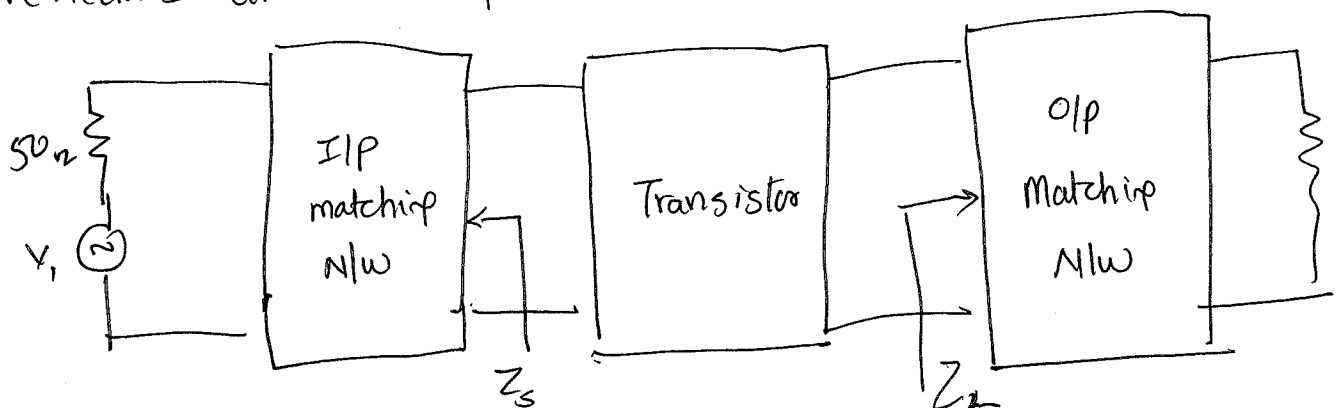
Solving these equations we get

$$R = 10 \Omega$$

$$L = 0.1024 \text{ nH} \quad C = 14.95 \text{ pF}$$

### IMPEDANCE MATCHING NETWORKS

When we study amplifiers matching N/ws play an important role for delivering maximum power to the output and preventing reflections at the input



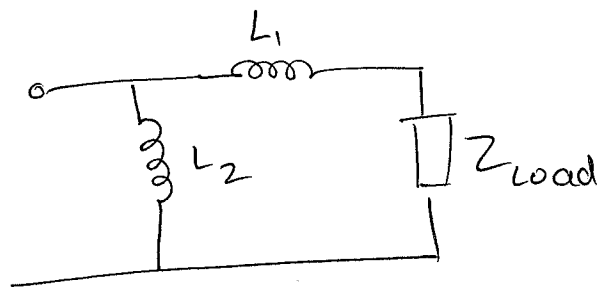
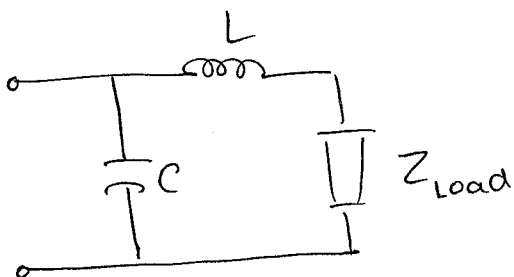
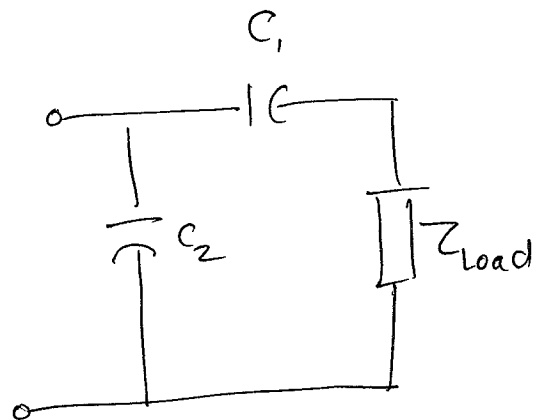
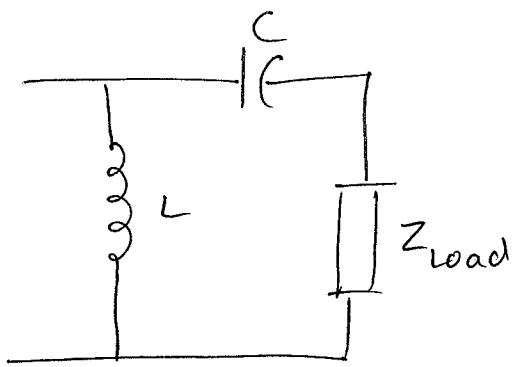
I/P matching N/w is used to transform the generator impedance to source impedance  $Z_s$

- O/P matching N/w is used to transform  $50\Omega$  to load impedance  $Z_L$

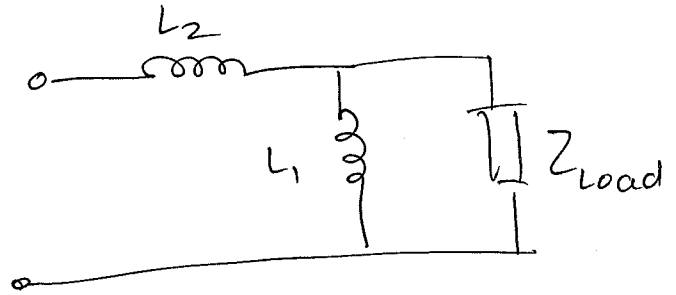
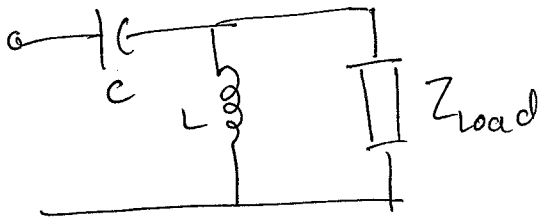
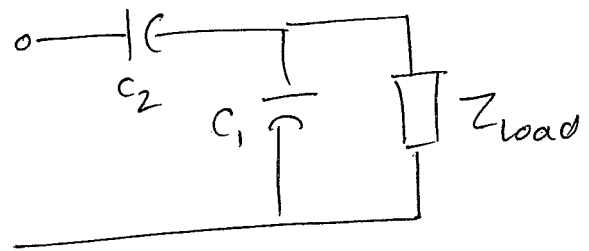
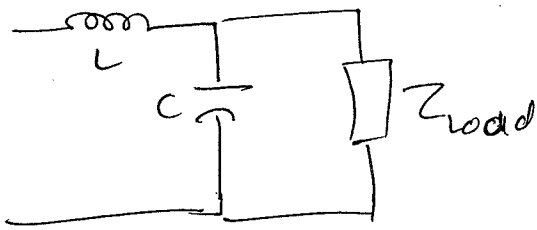
- Although many different matching N/ws can be designed, the eight ELL section (also denoted as L sections) are used more often. The matching N/ws are lossless in order not to dissipate any of the signal power.

The ZY smith chart can be used for designing the matching N/w.

Here are the 8 configurations





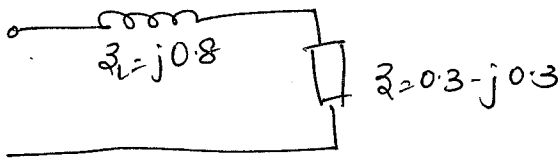


Now let's see what happens when we add a series reactance element to an impedance or a parallel susceptance element to an admittance in the  $ZY$  Smith chart.

① Let's see the effect of adding a series inductance  $L$  ( $Z_L = j0.8$ ) to an impedance  $Z = (0.3 - j0.3)$  (See Smith chart)

② Let's see the effect of adding a shunt inductor  $L$  ( $Y_L = -j2.4$ ) to an admittance  $Y$  ( $Y = 1.6 + j1.6$ ) on the  $ZY$  Smith chart (See Smith chart)

$$Z = 0.3 - j0.3$$



- Mark point A

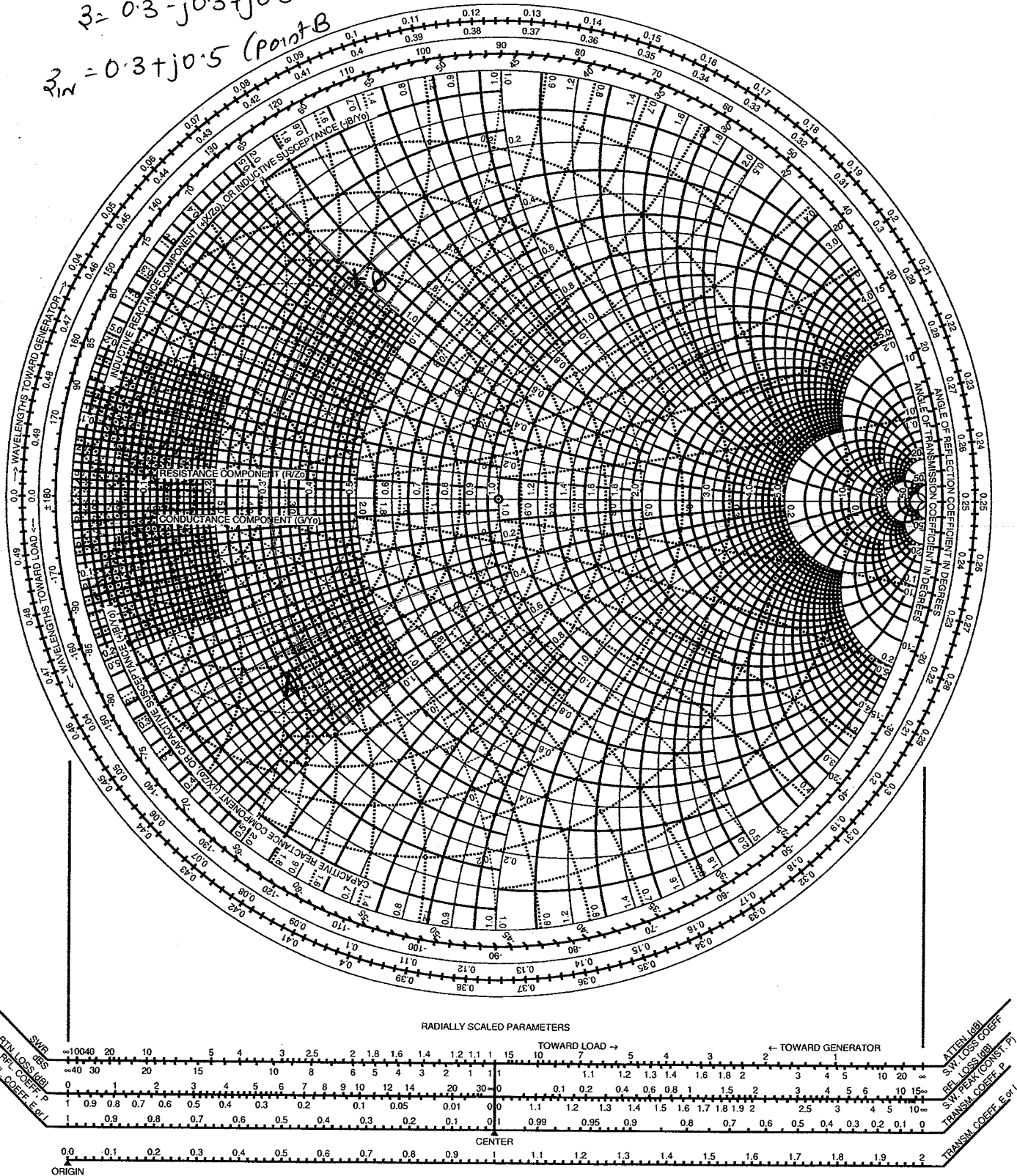
Add  $j = 0.8$

# The Complete Smith Chart (ZY)

this becomes

$$Z = 0.3 - j0.3 + j0.8$$

$$Z_{in} = 0.3 + j0.5 \text{ (point B)}$$



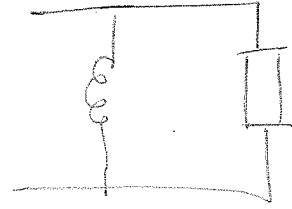
$$y = 1.6 + j1.6$$

mark point A

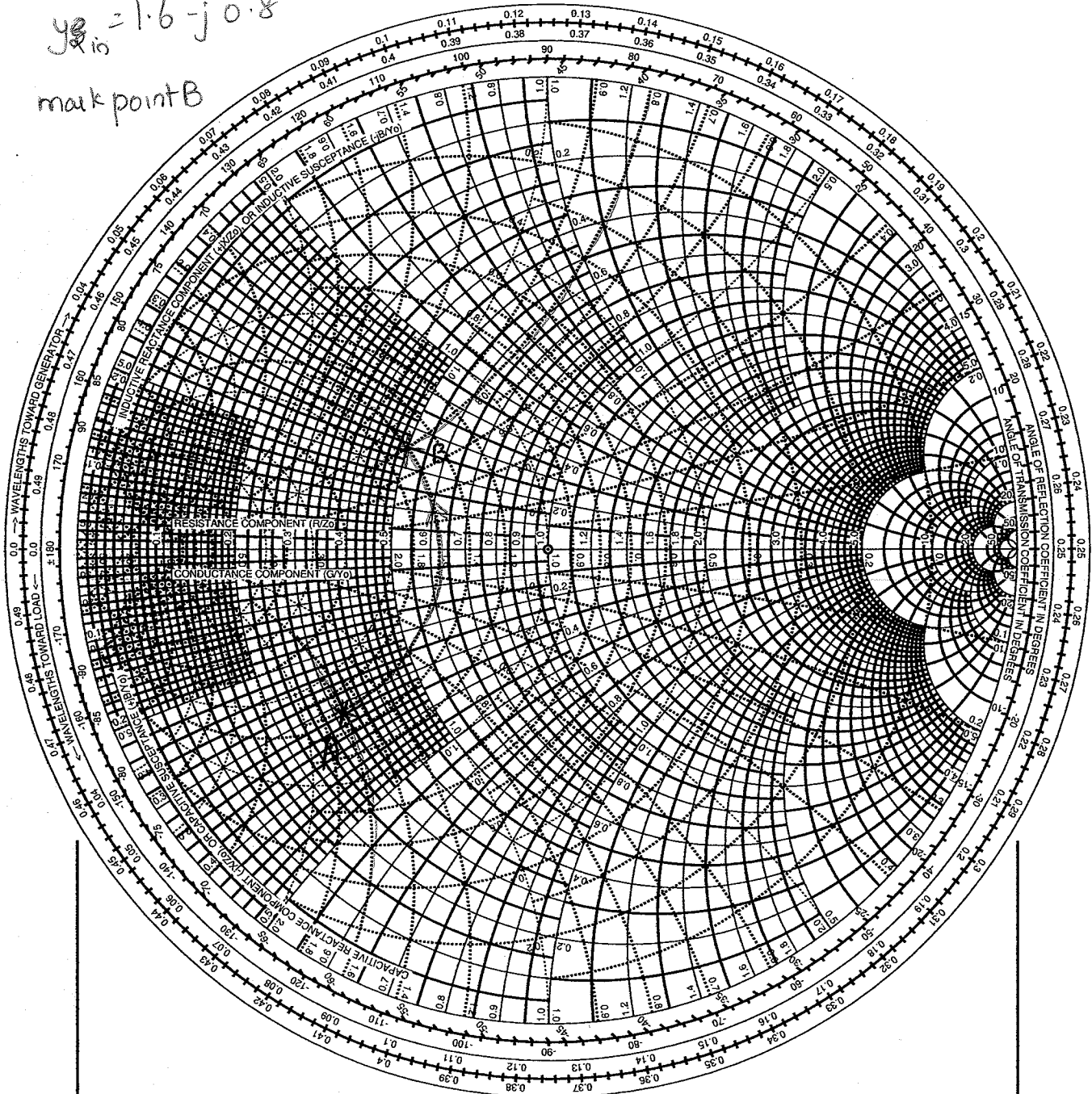
$$y = 1.6 + j1.6 - j2.4$$

$$y_{in} = 1.6 - j0.8$$

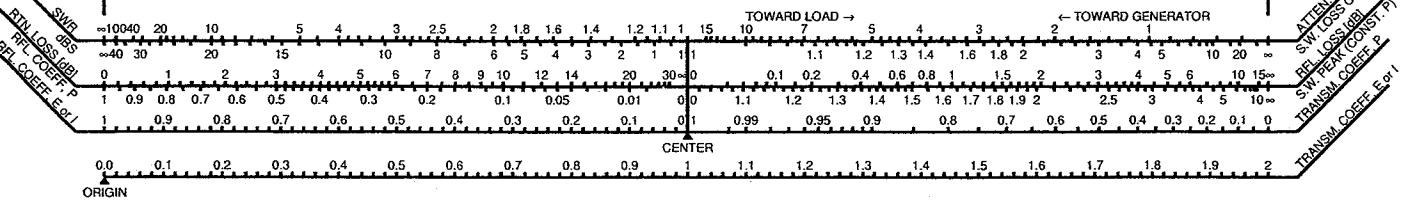
mark point B



# The Complete Smith Chart (ZY)



### RADIALLY SCALED PARAMETERS



- Adding a series inductance (reactance) produces a motion along a constant resistance circle in the  $ZY$  Smith chart, and adding shunt susceptance produces a motion along a constant conductance circle in the  $ZY$  Smith chart.

These are shown in figure 2.4.7

eg-  $Z_{load} = 10 + j10$  is to be matched to  $50 \Omega$  load. (See Smith chart)

$$Z_{load} = 0.2 + j0.2$$

Sometimes a specific matching N/w cannot be used to accomplish a given match.

- For example any load impedance falling in the marked region cannot be matched to  $50 \Omega$  with a network shown in the figure (see Smith chart) - II

- Second observation is that for the ELL matching Network only those with inductor and a capacitor can be used to provide a match between a resistive load and an input resistance.

$$Z = 0.2 + j0.2$$

Plot point A

## The Complete Smith Chart (ZY)

Series L - shunt C

$$Z_L = j0.4 - j0.2 = j0.2$$

see that B is along  
constant conductance  
the admittance at B is

$$Y_B = 1 - j0.2$$

- moving from  
B to C

$$Y_C = 0 - (-j2) = j2$$

$$Z_C = \frac{1}{j2} = -j0.5$$

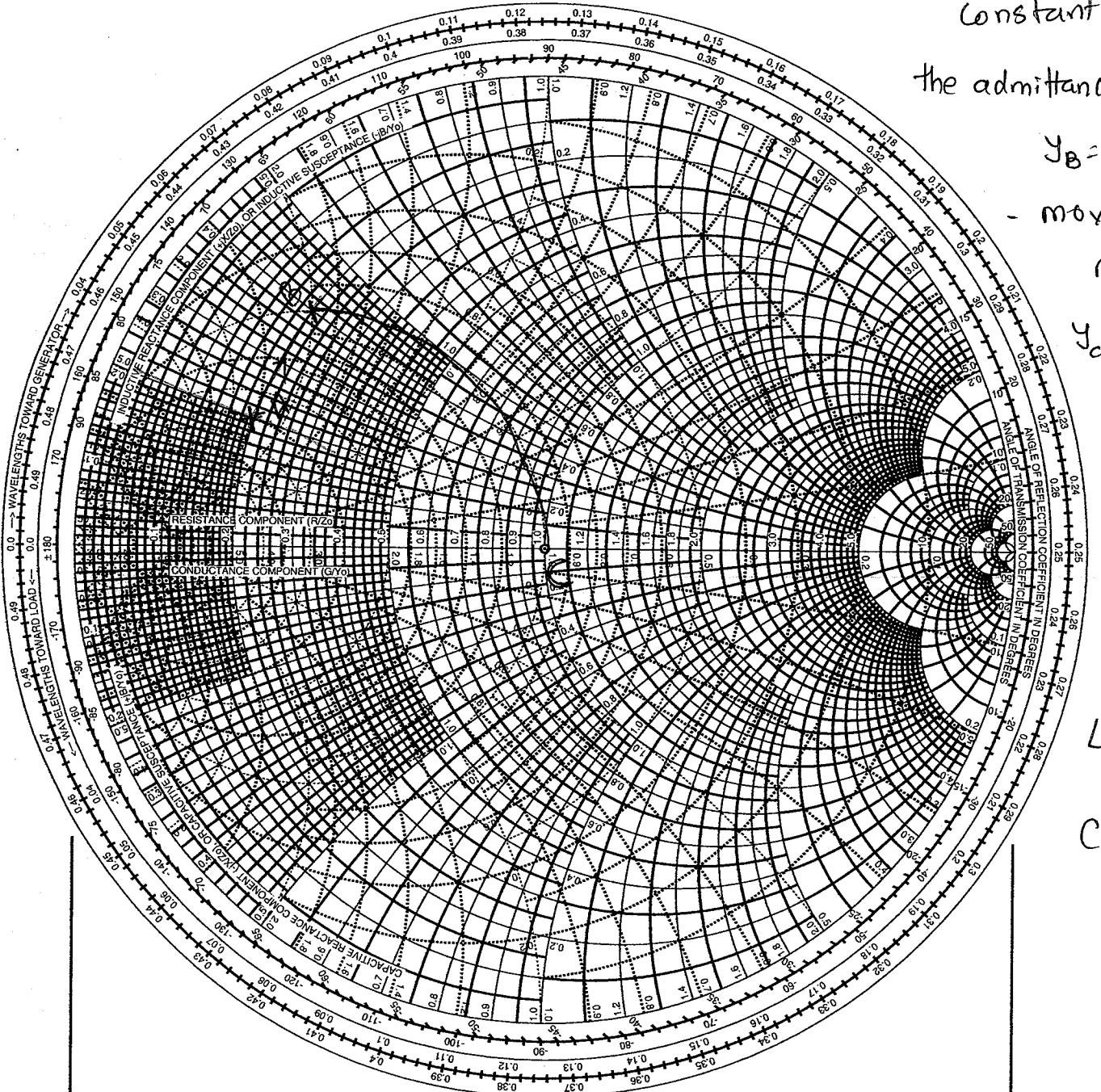
At point C

$$Y_{IN} = Z_{IN}^{-1} = 1$$

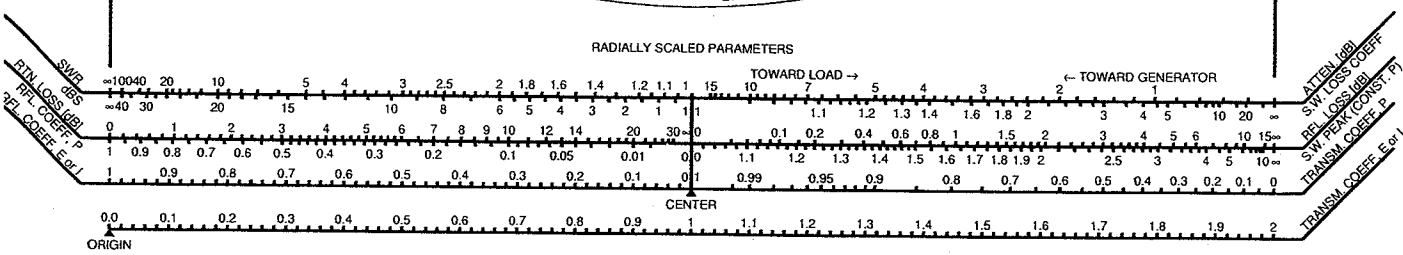
$$L = \frac{10}{2\pi f}$$

$$C = \frac{1}{2\pi f \times 25 \times f}$$

$$2\pi f \times 25 \times f$$

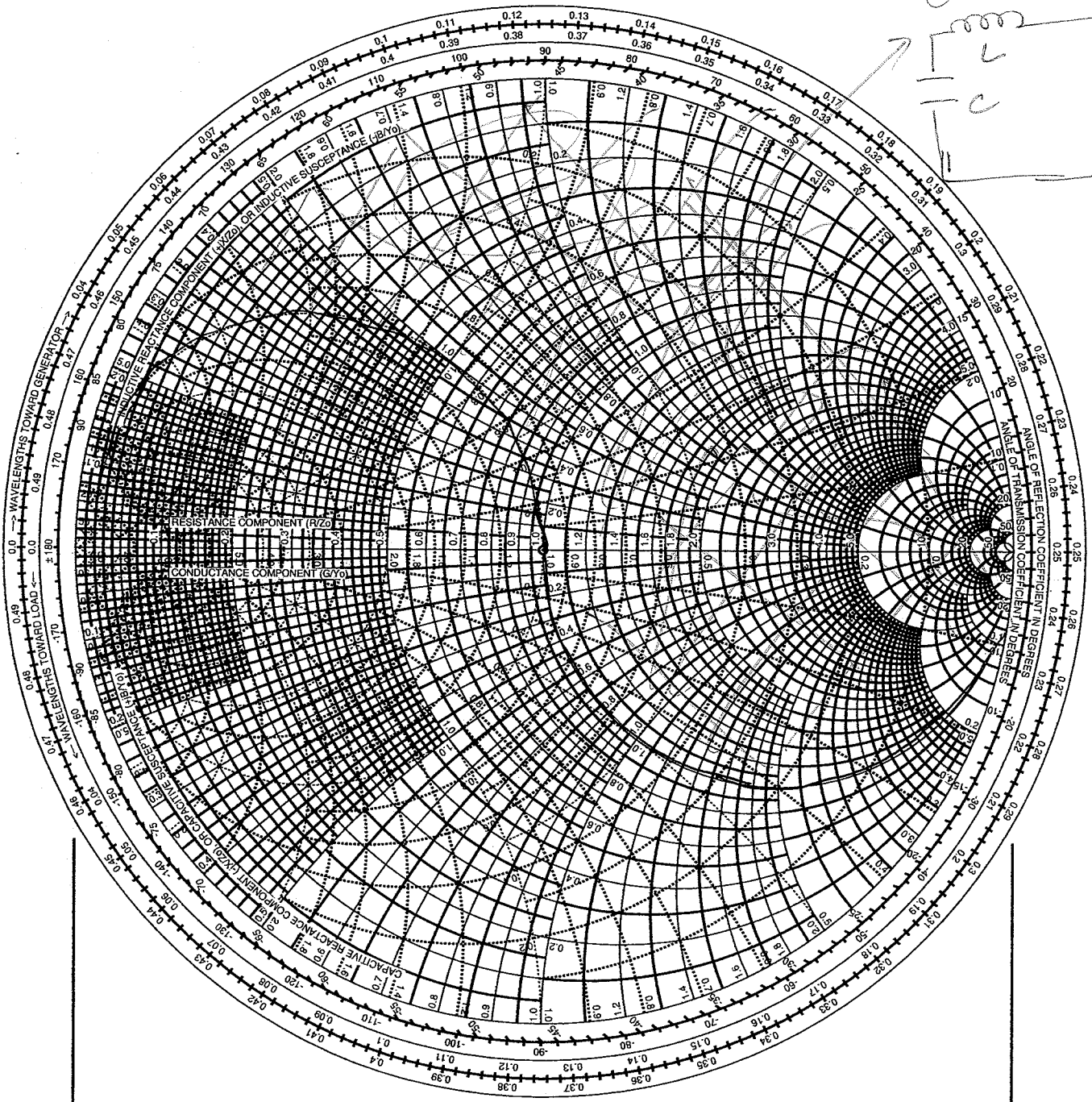
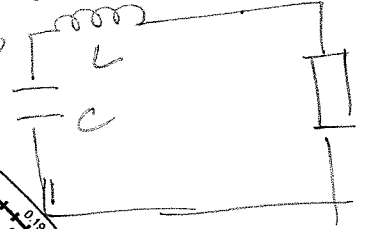


RADIALLY SCALED PARAMETERS

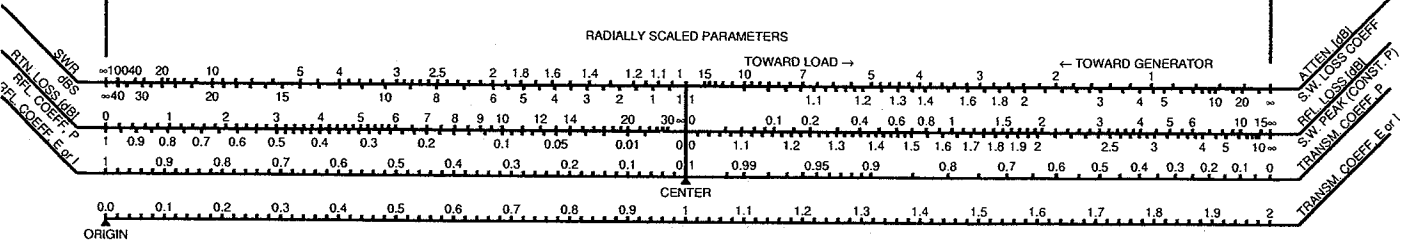


# The Complete Smith Chart (ZY)

*Cannot be used*



## RADIALLY SCALED PARAMETERS



In a resonant circuit, the ratio of its resonant frequency  $f_0$  to its bandwidth is known as the loaded  $Q$  of the circuit.

$$Q_L = \frac{\omega_0}{\text{BW}}$$

If BW is expressed in Hz

$$Q_L = \frac{f_0}{\text{BW}}$$

The ELL matching network is used for matching at a certain frequency. The frequency response of an ELL network can be classified as either a low pass filter or a high pass filter.

At each node of the ELL matching network, there is an equivalent series input impedance, denoted as  $R_s + jX_s$ .

Hence, a circuit node  $Q$ , denoted by  $Q_n$  can be defined at each node as

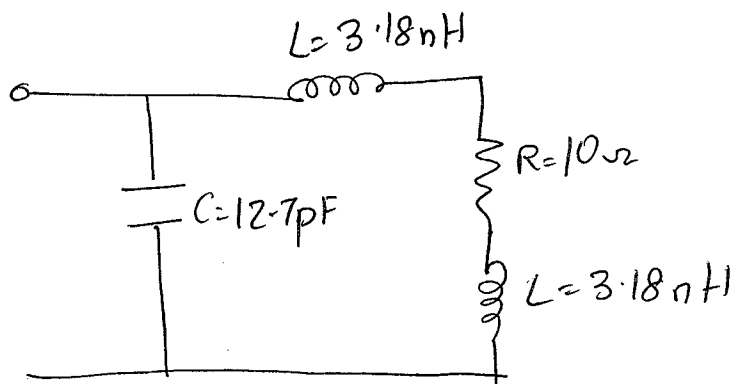
$$Q_n = \frac{|X_s|}{R_s} \quad - (1)$$

If the equivalent parallel input admittance at the node is  $G_p + jB_p$ , the circuit node  $Q$  can be expressed as

$$Q_n = \frac{|B_p|}{G_p}$$

-(2)

For eg. For the ckt shown below



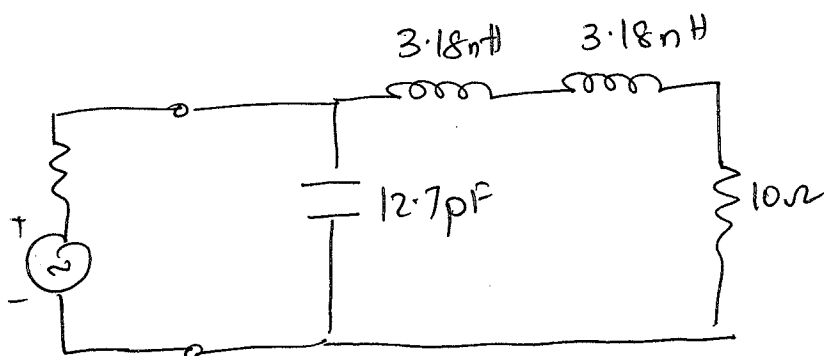
∴ Imp impedance of the circuit at point B is  $0.2 + j0.4$ .

∴ The ckt node Q is  $Q_n = \frac{0.4}{0.2} = 2$

The equivalent parallel admittance is readily found to be  $1 - j2$  producing ckt node Q, according to (2) can

be written as  $Q_n = \frac{2}{1} = 2$

The ckt can be written as.



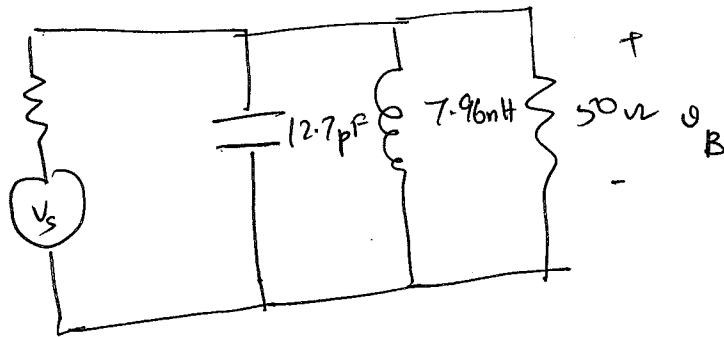


For a narrowband range of frequencies around  $f_0$ , the filter can be viewed as Bandpass filter with a loaded  $Q$  which can be calculated as

$$Q = \frac{f_0}{BW}$$

The equivalent bandpass filter is shown in figure below which is obtained by changing  $Z_B = 10 + j20 \Omega$  to an equivalent admittance (ie  $50 \Omega \parallel$  with  $j25$ )

The  $Q$  loaded can be given as



$$Q_L = \frac{\omega_0}{BW} = \omega_0 R_T C = 1$$

The relation between  $Q_L$  and  $Q_n$  is that

$$Q_L = \frac{Q_n}{2}$$