ECE 3510

Effect of initial conditions

See Bodson text, section 3.5

Best explained by example, IF:
$$\mathbf{H}(s) = \frac{b_2 \cdot s^2 + b_1 \cdot s + b_0}{s^2 + a_1 \cdot s + a_0} \cdot \mathbf{X}(s)$$

We would normally say:

$$\mathbf{Y}(s) = \frac{b_2 \cdot s^2 + b_1 \cdot s + b_0}{s^2 + a_1 \cdot s + a_0} \cdot \mathbf{X}(s)$$

But that ignores initial conditions. So let's deconstruct and then reconstruct with initial conditions included.

$$\mathbf{Y}(s) \cdot \left(s^2 + a_1 \cdot s + a_0\right) = \left(b_2 \cdot s^2 + b_1 \cdot s + b_0\right) \cdot \mathbf{X}(s)$$

$$s^{2} \cdot \mathbf{Y}(s) + a_{1} \cdot s \cdot \mathbf{Y}(s) + a_{0} \cdot \mathbf{Y}(s) = b_{2} \cdot s^{2} \cdot \mathbf{X}(s) + b_{1} \cdot s \cdot \mathbf{X}(s) + b_{0} \cdot \mathbf{X}(s)$$

$$\frac{d^2}{dt^2} y(t) + a_1 \cdot \frac{d}{dt} y(t) + a_0 \cdot y(t) = b_2 \cdot \frac{d^2}{dt^2} x(t) + b_1 \cdot \frac{d}{dt} x(t) + b_0 \cdot x(t)$$

Laplace Properties

Operation

$$\frac{\mathrm{d}}{\mathrm{d}t}\mathrm{f}(t)$$

$$\mathbf{s} \cdot \mathbf{F}(\mathbf{s}) - \mathbf{f}(0^{-})$$

$$\frac{d^2}{dt^2} \ f(t)$$

$$s^2 \cdot \mathbf{F}(s) - s \cdot f(0^-) - \frac{d}{dt} f(0^-)$$

$$\frac{d^{2}}{dt^{2}} y(t) + a_{1} \cdot \frac{d}{dt} y(t) + a_{0} \cdot y(t) = b_{2} \cdot \frac{d^{2}}{dt^{2}} x(t) + b_{1} \cdot \frac{d}{dt} x(t) + b_{0} \cdot x(t)$$

$$\left(s^2 \cdot \mathbf{Y}(s) - s \cdot \mathbf{y}(0^-) - \frac{d}{dt}\mathbf{y}(0^-)\right) + a_1 \cdot \left(s \cdot \mathbf{Y}(s) - \mathbf{y}(0^-)\right) + a_0 \cdot \mathbf{Y}(s)$$

$$b_{2} \cdot \left(s^{2} \cdot \mathbf{X}(s) - s \cdot x(0^{-}) - \frac{d}{dt}x(0^{-})\right) + b_{1} \cdot \left(s \cdot \mathbf{X}(s) - x(0^{-})\right) + b_{0} \cdot \mathbf{X}(s)$$

$$\left(s^2 \cdot \mathbf{Y}(s) + a_1 \cdot s \cdot \mathbf{Y}(s) + a_0 \cdot \mathbf{Y}(s)\right) - s \cdot y(0^-) - \frac{d}{dt}y(0^-) - a_1 \cdot y(0^-) = 0$$

$$\left(b_{2}\cdot s^{2}\cdot \boldsymbol{X}(s)+b_{1}\cdot s\cdot \boldsymbol{X}(s)+b_{0}\cdot \boldsymbol{X}(s)\right)-b_{2}\cdot s\cdot x\left(0^{-}\right)-b_{2}\cdot \frac{d}{dt}x\left(0^{-}\right)-b_{1}\cdot x\left(0^{-}\right)$$

$$\mathbf{Y}(s) \cdot \left(s^2 + a_1 \cdot s + a_0\right) = \left(b_2 \cdot s^2 + b_1 \cdot s + b_0\right) \cdot \mathbf{X}(s) + \left(s \cdot y(0^-) + \frac{d}{dt}y(0^-) + a_1 \cdot y(0^-) - b_2 \cdot s \cdot x(0^-) - b_2 \cdot \frac{d}{dt}x(0^-) - b_1 \cdot x(0^-)\right)$$

Response to input
$$\mathbf{Y}(s) = \frac{b_2 \cdot s^2 + b_1 \cdot s + b_0}{s^2 + a_1 \cdot s + a_0} \cdot \mathbf{X}(s) + \frac{s \cdot y(0^-) + \frac{d}{dt}y(0^-) + a_1 \cdot y(0^-) - b_2 \cdot s \cdot x(0^-) - b_2 \cdot \frac{d}{dt}x(0^-) - b_1 \cdot x(0^-)}{s^2 + a_1 \cdot s + a_0}$$

Forced response

Zero-state response

Natural response Zero-input response

ECE 3510 Effect of initial cond. p1

$$\mathbf{Y}(s) = \frac{b \cdot 2 \cdot s^2 + b \cdot 1 \cdot s + b \cdot 0}{s^2 + a \cdot 1 \cdot s + a \cdot 0} \cdot \mathbf{X}(s) + \frac{s \cdot y(0^-) + \frac{d}{dt}y(0^-) + a \cdot y(0^-) - b \cdot 2 \cdot s \cdot x(0^-) - b \cdot 2 \cdot \frac{d}{dt}x(0^-) - b \cdot 1 \cdot x(0^-)}{s^2 + a \cdot 1 \cdot s + a \cdot 0}$$

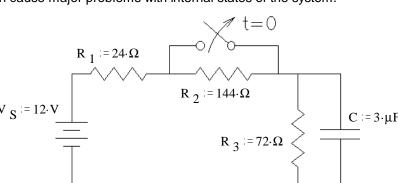
Observations

- 1. The total response is the sum of two independent components.
- 2. These values together fully describe the *state* of the 2nd-order system at time $t = 0^-$ (the initial state): $y(0^-) = \frac{d}{dt}y(0^-) = x(0^-) = \frac{d}{dt}x(0^-)$
- 3. Similar denominator for both parts = Share poles = Similar responses
- 4. Response to Initial conditions always go to zero if system is BIBO.
- 5. Pole-zero cancellations in right-half plane can cause major problems with internal states of the system.

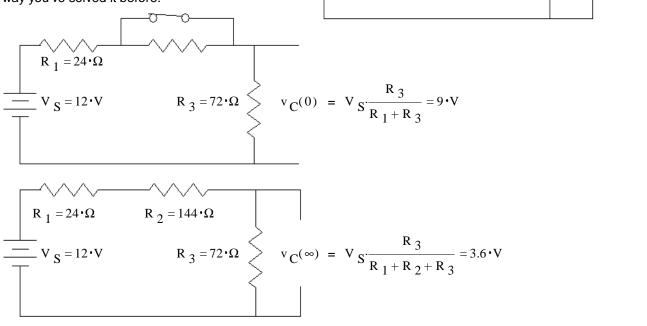
A simple first-order example

The switch has been closed for a long time and is opened at time t=0.

Find the complete expression for $\boldsymbol{v}_{\boldsymbol{C}}(t).$



The way you've solved it before:



$$R_{1} = 24 \cdot \Omega \qquad R_{2} = 144 \cdot \Omega$$

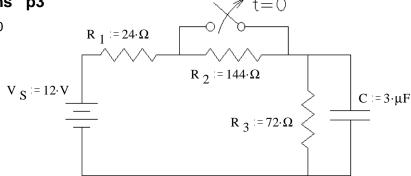
$$R_{3} = 72 \cdot \Omega \qquad R_{Th} := \frac{1}{\left(\frac{1}{R_{3}} + \frac{1}{R_{1} + R_{2}}\right)} \qquad R_{Th} = 50.4 \cdot \Omega$$

$$\tau := R_{Th} \cdot C \qquad \tau = 151.2 \cdot \mu s$$

$$v_{C}(t) = v_{C}(\infty) + \left(v_{C}(0) - v_{C}(\infty)\right) \cdot e^{\frac{-t}{\tau}} = 3.6 \cdot V + (9 \cdot V - 3.6 \cdot V) \cdot e^{\frac{-t}{151 \cdot \mu s}} = 3.6 \cdot V + 5.4 \cdot V \cdot e^{\frac{-t}{151 \cdot \mu s}}$$

ECE 3510 Effect of initial conditions p3

The way we would do the same thing in 3510



$$\begin{split} \mathbf{H}(s) &= \frac{\mathbf{V}_{\mathbf{C}}(s)}{\mathbf{V}_{\mathbf{S}}(s)} = \frac{\frac{1}{\frac{1}{R_3} + \mathbf{C} \cdot \mathbf{s}}}{\frac{1}{R_1 + R_2 + \frac{1}{\frac{1}{R_3} + \mathbf{C} \cdot \mathbf{s}}} \cdot \frac{\left(\frac{1}{R_3} + \mathbf{C} \cdot \mathbf{s}\right)}{\left(\frac{1}{R_3} + \mathbf{C} \cdot \mathbf{s}\right)} = \frac{1}{\frac{R_1 + R_2}{R_3} + \left(R_1 + R_2\right) \cdot \mathbf{C} \cdot \mathbf{s} + 1} \cdot \frac{\left[\frac{1}{\left(R_1 + R_2\right) \cdot \mathbf{C}}\right]}{\left[\frac{1}{\left(R_1 + R_2\right) \cdot \mathbf{C}}\right]} \\ &= \frac{1}{\frac{R_1 + R_2}{R_3} + \left(R_1 + R_2\right) \cdot \mathbf{C} \cdot \mathbf{s} + 1} \cdot \frac{\left[\frac{1}{\left(R_1 + R_2\right) \cdot \mathbf{C}}\right]}{\left[\frac{1}{\left(R_1 + R_2\right) \cdot \mathbf{C}}\right]} = \frac{\frac{1}{\left(R_1 + R_2\right) \cdot \mathbf{C}}}{\frac{1}{R_3 \cdot \mathbf{C}} + \frac{1}{\left(R_1 + R_2\right) \cdot \mathbf{C}}} \end{split}$$

First-order version of Y(s) with initial conditions

$$\mathbf{Y}(s) = \frac{b}{s+a} \frac{12 \cdot V}{s} + \frac{y(0-)}{s+a} \frac{b}{0} \frac{12 \cdot V}{s} = \frac{A}{s} + \frac{B}{s+a} \frac{A}{0} = \frac{\mathbf{H}(0) \cdot 12 \cdot V}{s} = \frac{b}{a} \frac{0}{0} \cdot 12 \cdot V = 3.6 \cdot V$$

$$\mathbf{B} = b \frac{12 \cdot V}{s} = \frac{b}{s} \frac{0}{s+a} \cdot 12 \cdot V = -3.6 \cdot V$$

$$\mathbf{B} = b \frac{12 \cdot V}{s} = \frac{b}{s} \cdot 12 \cdot V = -3.6 \cdot V$$

$$= \frac{3.6 \cdot V}{s} + \frac{-3.6 \cdot V}{s + a_0} + \frac{y(0^{-})}{s + a_0}$$

$$y(t) = V_C(t) = \left(3.6 \cdot V - 3.6 \cdot V \cdot e^{-a_0 \cdot t} + 9 \cdot V \cdot e^{-a_0 \cdot t}\right) \cdot u(t)$$

Same as above
$$v_C(t) = 3.6 \cdot V + (9 \cdot V - 3.6 \cdot V) \cdot e^{-\frac{t}{151 \cdot \mu s}}$$
 where $\tau = \frac{1}{a_0} = \frac{\sec}{6614} = 151.2 \cdot \mu s$

ECE 3510

State Space

A completely different method where all math is done in the time-domain using linear algebra. See Bodson, section 3.6.

x(t) = The state vector (n x 1 matrix)

 $\frac{d}{dt}x(t)$ = Time derivative of the state vector (n x 1 matrix)

n = order of the system

u(t) = The input vector $(n_u \times 1 \text{ matrix})$

y(t) = The state vector ($n_v \times 1$ matrix)

 n_u = number of inputs

 n_{v} = order of the system

A =The system matrix ($n \times n$ matrix)

B = The input matrix ($n \times n_{ij}$ matrix)

C = The output matrix $(n_v \times n \text{ matrix})$

D = The feed-forward matrix ($n_v \times n_{ij}$ matrix)

State Equation:

$$\frac{d}{dt}x(t) = A \cdot x(t) + B \cdot u(t)$$

A third-order, 2-input, 2-output system

$$\begin{pmatrix} \mathbf{1} \\ \mathbf{1} \\ \mathbf{1} \end{pmatrix} = \begin{pmatrix} \mathbf{1} & \mathbf{1} & \mathbf{1} \\ \mathbf{1} & \mathbf{1} & \mathbf{1} \end{pmatrix} \cdot \begin{pmatrix} \mathbf{1} \\ \mathbf{1} \\ \mathbf{1} \end{pmatrix} + \begin{pmatrix} \mathbf{1} & \mathbf{1} \\ \mathbf{1} & \mathbf{1} \end{pmatrix} \cdot \begin{pmatrix} \mathbf{1} \\ \mathbf{1} \\ \mathbf{1} \end{pmatrix}$$

Output Equation:

$$y(t) = C \cdot x(t) + D \cdot u(t)$$

$$\begin{pmatrix} \mathbf{I} \\ \mathbf{I} \end{pmatrix} = \begin{pmatrix} \mathbf{I} & \mathbf{I} & \mathbf{I} \\ \mathbf{I} & \mathbf{I} & \mathbf{I} \end{pmatrix} \cdot \begin{pmatrix} \mathbf{I} \\ \mathbf{I} \\ \mathbf{I} \end{pmatrix} + \begin{pmatrix} \mathbf{I} & \mathbf{I} \\ \mathbf{I} & \mathbf{I} \end{pmatrix} \cdot \begin{pmatrix} \mathbf{I} \\ \mathbf{I} \end{pmatrix}$$

State Equation:

$$\frac{d}{dt}x(t) = A \cdot x(t) + B \cdot u(t)$$

A third-order, single-input, single-output system

$$\begin{pmatrix} \mathbf{I} \\ \mathbf{I} \\ \mathbf{I} \end{pmatrix} = \begin{pmatrix} \mathbf{I} & \mathbf{I} & \mathbf{I} \\ \mathbf{I} & \mathbf{I} & \mathbf{I} \end{pmatrix} \cdot \begin{pmatrix} \mathbf{I} \\ \mathbf{I} \\ \mathbf{I} \end{pmatrix} + \begin{pmatrix} \mathbf{I} \\ \mathbf{I} \\ \mathbf{I} \end{pmatrix} \cdot \mathbf{u}(t)$$

Output Equation:

$$y(t) = C \cdot x(t) + D \cdot u(t)$$

$$y(t) = C \cdot x(t) + D \cdot u(t)$$

$$y(t) = (\mathbf{I} \cdot \mathbf{I}) \cdot \begin{pmatrix} \mathbf{I} \\ \mathbf{I} \end{pmatrix} + D \cdot u(t)$$

Advantages of the state-space method

Easily handles multiple inputs, multiple outputs and initial conditions

Can be used with nonlinear systems

Can be used with time-varying systems

Reveals unstable systems that have stable transfer functions (pole-zero cancellations). You can determine:

Controllability: State variables can all be affected by the input

Observability: State variables are all "observable" from the output

Basis of Optimal control methods

Advantages and disadvantages of the classical frequency-domain method used in this class

Simpler to understand and model interconnected systems.

Rapidly provide stability and transient response information.

Easy to see the effects of varying system parameters to get a good design.

Limited to linear, time-invariant systems or systems that can be approximated as such.