

## ECE 3510 Exam 3 Information

This sheet and the Information sheets from Exams 1 & 2 are the only reference materials allowed at exam. Bring this page.

You **may add** whatever you want to this sheet (both sides).

### Root-Locus Plots Additional Rules

The **breakaway/in points** are also solutions to: 
$$\sum_{\text{all}} \frac{1}{(s + p_i)} = \sum_{\text{all}} \frac{1}{(s + z_i)}$$

Phase angle of  $G(s)$  at any point on the root locus:  $\arg(G(s)) = \arg(N(s)) - \arg(D(s)) = \pm 180^\circ, \pm 540^\circ, \dots$

Or:  $\arg\left(\frac{1}{G(s)}\right) = \arg(D(s)) - \arg(N(s)) = \pm 180^\circ, \pm 540^\circ, \dots$   
 Note:  $\arg(x)$  is  $\angle(x)$

**Departure angle** ( $\theta_D$ ) from a complex pole ( $p_c$ ). Recall rule 9 (one of the most important rules):

for any point  $s$  on the root locus:  $\arg(G(s)) = \arg(N(s)) - \arg(D(s)) = \pm 180^\circ \pm 360^\circ \dots$

Imagine a point  $\epsilon$ -distance away from the complex pole. That point would have an angle of  $\theta_D$  with respect to the complex pole, but it's angle relative to all the other poles and zeros would be essentially the same as the complex pole.

$$\sum_{\text{all zeroes}} (\text{angle of point } s \text{ relative to zero}) - \sum_{\text{all poles but } p_c} (\text{angle of point } s \text{ relative to pole}) - \theta_D = \pm 180^\circ \pm 540^\circ \dots$$

all zeroes

all poles but  $p_c$

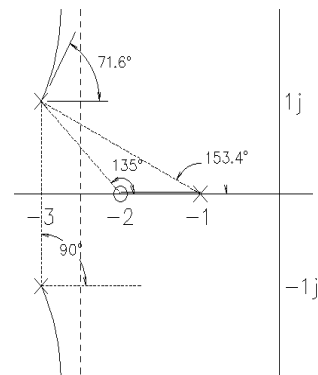
Example:  $G(s) := \frac{s+2}{(s+1) \cdot [(s+3)^2 + 1^2]}$

Find the departure angle

from the pole at:  $p_c := -3 + 1 \cdot j$

$$135 - 153.4 - 90 - \theta_D = \pm 180^\circ \pm 540^\circ \dots$$

rearrange:  $\theta_D = 180 - 90 - 153.4 + 135 = 71.6 \text{ deg}$



**Arrival angle** ( $\theta_A$ ) to complex zero ( $z_c$ ). Exactly the same idea.

### To create an unconventional root locus plot:

1. Determine the gain factor if it can be adjusted, and make it part of the open-loop transfer function,  $G(s)$ . Hold it constant at some number.
2. Determine the denominator of the closed-loop transfer function,  $H(s)$ . Let's call it  $D_H(s)$ .
3. Rearrange  $D_H(s)$  into this form:  $D'(s) + x \cdot N'(s)$  where  $x$  is the variable for which you want to draw the root locus. Notice that  $x$  occupies exactly the same position the gain would normally occupy. Normal:  $D_G(s) + k \cdot N_G(s)$   
 Note: If you cannot rearrange  $D_H(s)$  into this form, then you cannot use this method to create an root locus plot for the variable  $x$ .  
 Now:  $D'(s) + x \cdot N'(s)$
4. Now simply draw a root locus as though  $D'(s)$  was the open-loop denominator and  $N'(s)$  was the open-loop numerator.

## Root Locus Design

**PI** To eliminate steady-state error (for constant inputs) & perfect rejection of constant disturbances

Add pole at 0 and zero at close by

**LAG** An alternative is a Lag Compensator, with a pole near the origin and a zero a little further away.

**PD or PID** To Improve the dynamic response, add a zero to affect angles.

**LEAD** An alternative to the differentiator is a Lead Compensator with a zero and a pole much further left.

## Root Locus Design Crib Sheet

Using 2nd-order approximation:  $\frac{N(s)}{(s+a)^2 + b^2} = \frac{N(s)}{s^2 + 2 \cdot a \cdot s + a^2 + b^2} = \frac{N(s)}{s^2 + 2 \cdot \zeta \cdot \omega_n \cdot s + \omega_n^2}$

$$\omega_n^2 = a^2 + b^2 \quad \omega_n = \text{natural frequency}$$

$$\zeta \cdot \omega_n = a$$

$$\zeta = \frac{a}{\omega_n} = \frac{a}{\sqrt{a^2 + b^2}} = \text{damping factor}$$

$$\zeta = \sin\left(\text{atan}\left(\frac{a}{b}\right)\right)$$

Overshoot:  $OS = e^{-\frac{\pi \cdot a}{b}} \quad \%OS = 100\% \cdot e^{-\frac{\pi \cdot a}{b}} \quad \frac{a}{b} = \frac{\ln(OS)}{-\pi}$

2% settling time:  $T_s = \frac{4}{a} = \frac{4}{\zeta \cdot \omega_n}$   $\%OS = 100\% \cdot e^{\frac{-\zeta \cdot \pi}{\sqrt{1-\zeta^2}}}$   $\zeta = \frac{-\ln(OS)}{\sqrt{\pi^2 + (\ln(OS))^2}}$

Weird forms from Nise book

Static error constant (position):  $K_p = \lim_{s \rightarrow 0} K \cdot C(s) \cdot G(s) \quad e_{\text{step}}(\infty) = e_{\text{step}} = \frac{1}{1 + K_p}$

Lag compensation improves  $K_p$ ,  $K_v$  and  $K_a$  by  $\frac{z_c}{p_c}$   $IE: K_{pc} \simeq K_{puc} \cdot \frac{z_c}{p_c}$

angle of constant damping line:  $90\text{-deg} + \text{atan}\left(\frac{a}{b}\right)$

## Bode Plots

Sample transfer function:

$$P(s) = K \cdot \frac{(s+z_1) \cdot (s+z_2)}{s \cdot (s+p_1) \cdot (s+p_2)^2}$$

Replace all s's with blanks:

$$P(\_) = K \cdot \frac{(\_+z_1) \cdot (\_+z_2)}{\_ \cdot (\_+p_1) \cdot (\_+p_2) \cdot (\_+p_2)}$$

Initial magnitude =  $K \cdot \frac{z_1 \cdot z_2}{(j \cdot \omega_{\text{start}}) \cdot p_1 \cdot (p_2) \cdot (p_2)}$

$\omega$ 's in num --> +20dB/dec each,  $j \Rightarrow 90^\circ$ ,  $- \Rightarrow +180^\circ$

$\omega$ 's in den --> -20dB/dec each,  $j \Rightarrow -90^\circ$ ,  $- \Rightarrow -180^\circ$

Cross out each pole or zero in turn & replace with  $j\omega$   $K \cdot \frac{(\_+z_1) \cdot (\_+z_2)}{(j\omega) \cdot (j\omega + \mathbf{X}_1) \cdot (\_+p_2) \cdot (\_+p_2)}$

zeros turn up the slope --> +20dB/decade

zeros increase the phase angle --> +90deg

poles turn down the slope --> -20dB/decade

poles decrease the phase angle --> -90deg

Draw a smooth line through the bode plots to estimate the actual magnitude and phase.

Actual magnitude: -3dB at single poles  
+3dB at single zeros

-6dB at double poles  
+6dB at double zeros etc..

Magnitude effects extend about 1 decade fore and aft.

Angle effects extend about 1.5 decade fore and aft. It is helpful to draw a line from 1 decade before to 1 decade after.