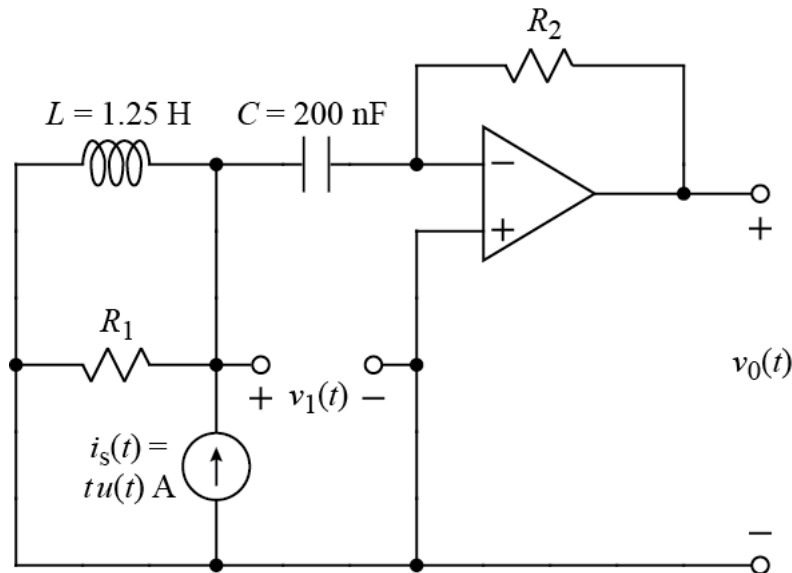


Ex:



The current source in the above circuit is off for $t < 0$.

- Find a symbolic expression for the Laplace-transformed output, $V_o(s)$, in terms of not more than R_1 , R_2 , L , C , and values of sources or constants.
- Choose a numerical value for R_1 for the circuit in problem 1 to make

$$v_1(t) = v_m - v_m e^{-\alpha t} \left[\cos(\beta t) + \frac{1}{2} \sin(\beta t) \right]$$

where v_m , α , and β are real-valued constants.

Hint: C behaves as though it is in parallel with L and R_1 .

sol'n: a) We define $\mathbb{I}(s)$ to the current flowing thru C toward the minus input of the op-amp. Since $\mathbb{I}(s)$ cannot flow into the op-amp, it also flows thru R_2 .

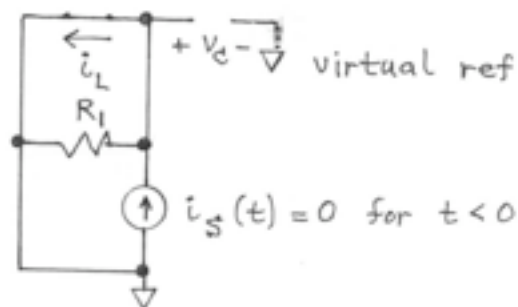
We can add a reference on the bottom rail, making V_+ at the positive input of the op-amp equal to $0V$. Because of R_2 and the negative feedback it provides, we have

$$V_- = V_+ = 0V$$

Given the direction of $\mathbb{I}(s)$ and $v_- = 0V$,
 Ohm's law gives the value of $V_o(s)$:

$$V_o(s) = -\mathbb{I}(s) R_2$$

To find $\mathbb{I}(s)$, we need initial conditions
 for L and C. We consider time $t=0^-$:



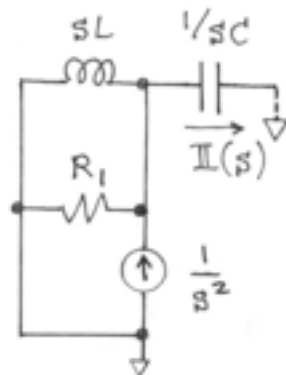
Since there is no current, we have

$$i_L(0^-) = 0, \quad v_e(0^-) = 0.$$

Thus, our initial conditions are zero.

The Laplace transform of $i_s(t)$ for $t > 0$ is

$$\mathcal{L}\{tu(t)A\} = \frac{1}{s^2}$$



R_1 , L , and C are effectively in parallel.

Thus, we have an \mathbb{I} -divider.

$$\begin{aligned}\mathbb{I}(s) &= \frac{1}{s^2} \frac{R_1 \parallel sL}{R_1 \parallel sL + \frac{1}{sC}} \\ &= \frac{1}{s^2} \frac{1}{1 + \frac{1}{sC} \left(\frac{1}{R_1} + sL \right)}\end{aligned}$$

$$\mathbb{I}(s) = \frac{1}{s^2 + \frac{1}{R_1 C} s + \frac{1}{LC}}$$

Now we can write an expression for $V_o(s)$:

$$V_o(s) = \frac{-R_2}{s^2 + \frac{1}{R_1 C} s + \frac{1}{LC}}$$

- b) The Laplace transform of $v_1(t)$, as specified in the problem, is as follows:

$$\begin{aligned}\mathcal{L}\{v_1(t) = v_m - v_m e^{-\alpha t} \left[\cos \beta t - \frac{1}{2} \sin \beta t \right]\} \\ = \frac{v_m}{s} - v_m \frac{(s+\alpha) + \frac{1}{2} \beta}{(s+\alpha)^2 + \beta^2} = V_1(s)\end{aligned}$$

For the circuit, using $\mathbb{I}(s)$ from part (a), we have the following for $V_1(s)$:

$$V_1(s) = \mathbb{I}(s) \frac{1}{sC} = \frac{1/C}{s \left(s^2 + \frac{1}{R_1 C} s + \frac{1}{LC} \right)}$$

To equate the two expressions for $V_1(s)$, we use a common denominator.

$$V_1(s) = V_m \left[\frac{\overset{\text{ii}}{(s+\alpha)^2 + \beta^2 - s(s+\alpha) - \beta/2}}{s(s^2 + 2\alpha s + \alpha^2 + \beta^2)} \right]$$

We now match the coefficients of each power of s for both the numerator and denominator.

coeff	expressions		
s^2	$0 = 0$	✓	(1)
s	numerator $V_m(2\alpha - \alpha - \beta/2) = 0$		(2)
1		$V_m(\alpha^2 + \beta^2) = 1/C$	(3)
$s \cdot s^2$	$1 = 1$		(4)
$s \cdot s$	denominator $2\alpha = \frac{1}{R_1 C}$		(5)
$s \cdot 1$		$\alpha^2 + \beta^2 = \frac{1}{LC}$	

From the last eq'n and the 3rd eq'n, we have

$$V_m(\alpha^2 + \beta^2) = V_m \frac{1}{LC} = 1/C$$

From the 5th eq'n we have an expression for α :

$$\alpha = \frac{1}{2R_1 C}$$

From the 2nd eq'n we have an expression for β in terms of α :

$$\alpha - \beta/2 = 0 \Rightarrow \beta = 2\alpha$$

Using this expression for β , we substitute into the 6th eq'n to find R_1 :

$$\alpha^2 + (2\alpha)^2 = \frac{1}{LC} \Rightarrow 5\alpha^2 = \frac{1}{LC}$$

or $5 \left(\frac{1}{2R_1 C} \right)^2 = \frac{1}{LC}$

or $\frac{5}{4R_1^2 C^2} = \frac{1}{LC}$

or $\frac{4}{5} R_1^2 C = L$

or $R_1^2 = \frac{5L}{4C}$

or $R_1 = \sqrt{\frac{5L}{4C}} = \sqrt{\frac{5\left(\frac{5}{4}\right)}{4 \cdot 200n}} \Omega$

or $R_1 = \frac{5}{4} \sqrt{5M} \Omega$

$R_1 = \frac{5\sqrt{5}}{4} k\Omega \approx 2.8 k\Omega$