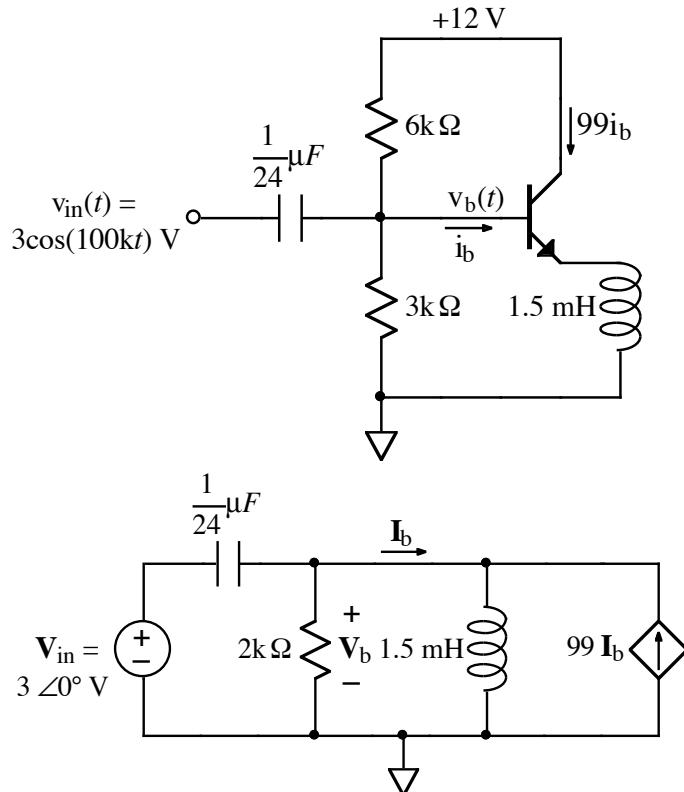




Ex:

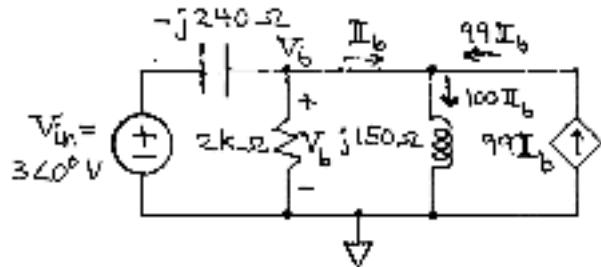


The above circuit diagrams show an emitter-follower amplifier and its high-frequency equivalent circuit. Find $v_b(t)$.

sol'n: The bottom diagram uses a mixed notation in that the C and L values are shown instead of $\frac{1}{\omega C}$ and $\frac{1}{\omega L}$. We first compute $\frac{1}{\omega C}$ and $\frac{1}{\omega L}$ using $\omega = 100k$ from the top circuit.

$$\frac{1}{\omega C} = \frac{1}{j\omega C} = -\frac{j}{\omega C} = -\frac{j}{100k \cdot \frac{1}{24} \mu} = -j 240 \Omega$$

$$Z_L = j\omega L = j 100k \cdot 1.5mH = j150\Omega$$



A straightforward solution approach is to use the node-voltage method with V_b on the top rail.

$$\frac{V_b - V_{in}}{-j240\Omega} + \frac{V_b}{2k\Omega} + \frac{V_b}{j150\Omega} - \frac{1}{100} = 0A$$

$$\text{or } V_b \left(\frac{1}{-j240\Omega} + \frac{1}{2k\Omega} + \frac{1}{j150\Omega} \right) = \frac{V_{in}}{-j240\Omega}$$

$$\text{or } V_b = \frac{V_{in}}{-j240\Omega} \cdot -j240\Omega \parallel 2k\Omega \parallel j150\Omega$$

$$\text{or } V_b = V_{in} \cdot 1 \parallel \frac{2k\Omega}{-j240\Omega} \parallel \frac{-j150\Omega}{240\Omega}$$

$$\text{Now } 1 \parallel \frac{-j150\Omega}{240\Omega} = \frac{1(-j150\Omega)}{240} = \frac{-j150\Omega}{240+j150\Omega}$$

$$\text{"} = \frac{j150\Omega}{14.76k} = \frac{j15}{14.76}$$

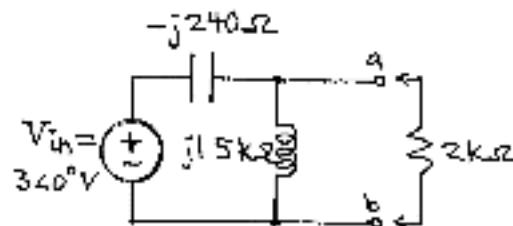
$$\begin{aligned}
 V_b &= V_{in} + \frac{15}{14.76} \left| \frac{-j25}{-j240} \right| \\
 &= V_{in} + \frac{15}{14.76} \left| \frac{j25}{3} \right| \\
 &= 3 \angle 0^\circ V + \frac{\frac{15}{14.76} \cdot j \frac{25}{3}}{\frac{15}{14.76} + j \frac{25}{3}} \\
 &= 3 \angle 0^\circ V + \frac{j \frac{1.5(25)}{3(15) + j 25(14.76)}}{3 + j 5(14.76)} \\
 &= 3 \angle 0^\circ V + \frac{j \frac{3(25)}{3 + j 5(14.76)}}{3 + j 73.8} \\
 &= 3 \angle 0^\circ V + \frac{j \frac{75}{9 + j 73.8}}{9 + j 73.8} \\
 &= \frac{22.5 \angle 90^\circ V}{\sqrt{9^2 + 73.8^2} \angle \tan^{-1} \frac{73.8}{9}} \\
 &\approx \frac{22.5 \angle 90^\circ V}{74.3 \angle 83.0^\circ} \\
 &\approx 3.02 \angle 90^\circ - 83.0^\circ V
 \end{aligned}$$

$$V_b \approx 3 \angle 7^\circ V$$

$$\therefore v_b(t) \approx 3 \cos(100kt + 7^\circ) V$$

An alternate approach begins with the observation that the L and the dependent source may be replaced by $j\omega L \cdot 100$. This concept is called "impedance multiplication".

Then we remove the $2k\Omega$ resistor and find the Thevenin equivalent of the circuit with respect to the terminals where the $2k\Omega$ resistor is attached.



$$V_{Th} = V_{a,b \text{ no load}}$$

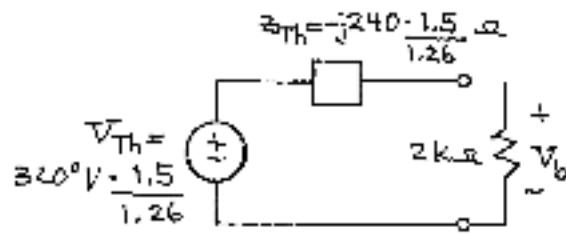
$$= V_{in} \cdot \frac{j1.5k\Omega}{j1.5k\Omega - j240\Omega}$$

$$V_{Th} = 3<40^\circ V \cdot \frac{15}{14.76}$$

$\underline{z}_{Th} = \underline{z}$ seen looking into a,b with V_{in} off (= wire)

$$\underline{z}_{Th} = -j240 \parallel j1.5k \Omega$$

$$\underline{z}_{Th} = \frac{240(1.5k)\Omega}{j(1.5k - 240)} = -j240 \cdot \frac{1.5}{14.76} \Omega$$



$$V_b = V_{Th} \cdot \frac{2k\Omega}{2k\Omega + Z_{Th}}$$

$$\approx 340^\circ V \cdot \frac{1.5}{14.76} \cdot \frac{2k\Omega}{2k\Omega - j240 \cdot \frac{1.5}{1.26} \Omega}$$

$$\approx 340^\circ V \cdot \frac{1.5 (2k\Omega)}{14.76 (2k\Omega) - j240 (1.5) \Omega}$$

$$= 340^\circ V \cdot \frac{30k}{29.52k - j36k}$$

$$= 340^\circ V \cdot \frac{30}{29.52 - j3.6}$$

$$= 340^\circ V \cdot \frac{1}{0.984 - j0.12}$$

$$= \frac{340^\circ V}{0.99 \angle -6.15^\circ}$$

$$V_b \approx 347^\circ V$$

$$\therefore v_b(t) = 3 \cos(100kt + 7^\circ) V$$