I (mA) 100

#### Stuff

#### Exam 2: Friday 3/7/03

PSpice 9.1 is available on computers in the lab, but regular labs take priority. PSpice 9.1 is also available in the 1st floor computers lab in EMCB 130. Look under "class software".

Note for Fig. 4.8 in text: i<sub>R</sub> should flow out of transistor.

**HW #14, due: F, 3/7** Ex3.13-15 (Note: units of

 $D_n \& D_n$  are wrong in Ex3.15)

**HW #15, due: W, 3/12** prob. 4.2 (ans:  $\beta$  = 368,122,24.2), Ex. 4.1 - 4.7 or see hw 15-16 handout

Assume  $V_T = 25 \text{mV}$ **HW #16, due: F, 3/14** Hw 15-16 handout

TA office hours, so that you can ask questions, retrieve HW etc: (Also shown on the bottom of the HW web page)

Andy Laraway In lab: W, 2:00 - 3:00 pm & F, 11:50 - 3:50 pm Greg Hill In lab: W, 7:30 - 8:30 am &W, 3:05 - 6:05 pm

Chakradhar Talluri In lab: W, 1:00 - 2:00 pm & H, 7:30 - 10:30 am & H, 2:00 - 5:00 pm

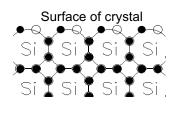
Zafeer Mohamed In lab: T, 7:30 - 10:30 am

Note: At lab times (the 3hr blocks) TAs will attend to lab students first.

## Reverse Bias Diode Leakage

The reverse leakage in a diode will actually be much larger than I<sub>s</sub>.

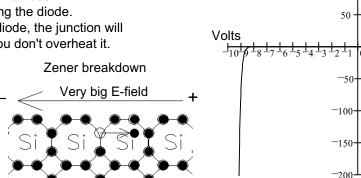
Any imperfection in the silicon crystal can lead to extra carriers and corresponding leakage current. The surface of the crystal can be seen as a large imperfection and can lead to significant "surface leakage". During manufacturing, "surface passivation" techniques can help clean up these loose bonds.

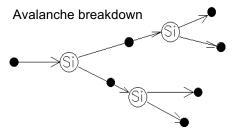


## **Diode Reverse Breakdown** section 3.3.4, p149 in textbook

One last diode property we ought to look at before leaving the diode. If you place a large enough reverse voltage across the diode, the junction will "break down". This will not harm the diode as long as you don't overheat it.

Breakdown occurs in two different ways.





Naturally occurring minority carriers gain so much speed that they can ionize other atoms when they hit, causing an "avalanche".

Dominant mechanism in zener diodes that break down above ~7V. Has a positive temperature coefficient.

E-field "rips" electrons out of position, creating carriers.

Dominant mechanism in zener diodes that break down below ~5V (because they are very heavily doped and have very narrow depletion regions). Has a negative temperature coefficient.

The most temperature-stable zener diodes have  $v_7$  between 5 & 7V (5.6V is very good).

If temperature stability is important, two 6V zeners in series are better than one 12V zener.

#### **Bipolar Junction Transistor** Notice how the base-emmitter junction is just like a diode. Small signal emitter resistance

Important relations (active region)

$$v_{BE} = 0.7 \cdot V$$
  $i_{C} = \beta \cdot i_{B}$ 

$$i_C = \beta \cdot i_B$$
  $i_E = i_B + i_C - i_C$   $V_{T} - 25 \cdot mV$ 

$$r_e = \frac{V_T}{I_C}$$

# Relations of lesser importance

$$i_C = \alpha \cdot i_E$$
  $\alpha = \frac{\beta}{\beta + 1}$   $\beta = \frac{\alpha}{1 - \alpha}$ 

Ebers-Moll equation: 
$$i_C = I_{S} e^{V_T}$$

relations of lesser importance 
$$i_{C} = \alpha \cdot i_{E} \qquad \alpha = \frac{\beta}{\beta + 1} \qquad \beta = \frac{\alpha}{1 - \alpha} \qquad \text{Temperature dependencies} \\ v_{BE} = 0.7 \cdot V \text{ (decreases about 2.1 mV / °C)} \\ \text{at constant I}_{C}: \quad \Delta V_{BE} = \frac{-2.1 \cdot \text{mV}}{\text{degC}}$$

at constant V<sub>BF</sub>: I<sub>C</sub> increases by 8% per °C (10x per 30°C)

## Bipolar Junction Transistor (BJT) DC and bias in the active region

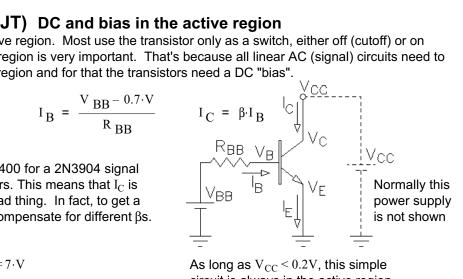
Few DC circuits use the transistor in its active region. Most use the transistor only as a switch, either off (cutoff) or on (saturation). Never-the-less the DC active region is very important. That's because all linear AC (signal) circuits need to use the transistor in its active (partially on) region and for that the transistors need a DC "bias"

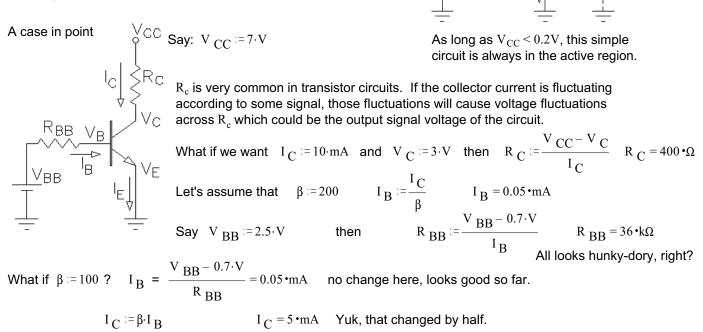
The simplest DC circuit:

The base current  $(I_B)$  is nice and stable, unfortunately this is more often a bad thing instead of a good thing.

$$I_B = \frac{V_{BB} - 0.7 \cdot V}{R_{BB}}$$

You see, β can be anything from 100 to 400 for a 2N3904 signal transistor, and that's normal for transistors. This means that  $I_{\rm C}$  is not stable, and that is almost always a bad thing. In fact, to get a stable  $I_C$ ,  $I_B$  will have to adjust itself to compensate for different  $\beta s$ .





Say: 
$$V_{CC} = 7.V$$

What if we want 
$$I_C := 10 \cdot \text{mA}$$
 and  $V_C := 3 \cdot V$  then  $R_C := \frac{V_{CC} - V_{C}}{I_{C}}$   $R_C = 400 \cdot \Omega$ 

Let's assume that 
$$\beta = 200$$

$$I_B := \frac{I_C}{\beta}$$
  $I_B = 0.05 \cdot mA$ 

Say 
$$V_{BB} := 2.5 \cdot V$$

$$R_{BB} := \frac{V_{BB} - 0.7}{I_{-}}$$

$$R_{BB} = 36 \cdot k\Omega$$

$$I_C := \beta \cdot I_E$$

$$I_{\alpha} = 5 \cdot m \Delta$$

$$\begin{split} & I_C \coloneqq \beta \cdot I_B & I_C = 5 \cdot \text{mA} & \text{Yuk, that changed by half.} \\ & V_C \coloneqq V_{CC} - I_C \cdot R_C & V_C = 5 \cdot V & \text{At least } V_C \text{ only changed by } 2V. \text{ Still, that may be too much.} \end{split}$$

At least we're still in the active region ( $V_{CE} > 0.2V$ ).

$$I_C := \beta \cdot I_E$$

$$I_C = 20 \cdot mA$$
 Oh oh, that doubled.

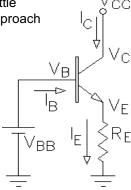
$$V_C := V_{CC} - I_{C} \cdot R_{CC}$$

 $I_C := \beta \cdot I_B \qquad \qquad I_C = 20 \cdot \text{mA} \quad \text{On on, that dodd}.$   $V_C := V_{CC} - I_C \cdot R_C \qquad \qquad V_C = -1 \cdot V \quad \text{Oops, that can't be good. In fact, we have to assume that we're out of the active region -- way bad...}$ 

Must recalculate 
$$\rm I_{C}$$
 and  $\rm V_{C}, \quad \rm V_{C} \coloneqq 0.2 \cdot \rm V \quad \text{(Saturation)}$ 

$$\text{Must recalculate I}_{C} \text{ and V}_{C}. \quad \text{V}_{C} \coloneqq 0.2 \cdot \text{V} \quad \text{(Saturation)} \qquad \text{I}_{C} \coloneqq \frac{\text{V}_{C}\text{C}^{-0.2} \cdot \text{V}}{\text{R}_{C}} \qquad \text{I}_{C} \equiv 17 \cdot \text{mA}$$

Let's try a little different approach



Again, let's design for 
$$I_C := 10 \cdot \text{mA}$$

$$V_E := V_{BB} - 0.7 \cdot V$$
 It is common here to assume:

$$R_E := \frac{V_E}{I_E} \qquad \qquad R_E = 180 \cdot \Omega$$

but actually, 
$$I_C = \alpha \cdot I_E = \frac{\beta}{\beta + 1} \cdot I_E$$

Again, let's design for 
$$I_C := 10 \cdot \text{mA}$$
 $V_E := V_{BB} - 0.7 \cdot \text{V}$  It is common here to assume:  $I_E := I_C$ 
 $R_E := \frac{V_E}{I_E}$   $R_E = 180 \cdot \Omega$   $I_E = 10 \cdot \text{mA}$ 

but actually,  $I_C = \alpha \cdot I_E = \frac{\beta}{\beta + 1} \cdot I_E$ 

If  $\beta := 100$   $\alpha := \frac{\beta}{\beta + 1}$   $I_C = \alpha \cdot I_E = 9.901 \cdot \text{mA}$   $I_B = \frac{I_C}{\beta} = 0.025 \cdot \text{mA}$ 

If  $\beta := 400$   $I_C = \frac{\beta}{\beta + 1} \cdot I_E = 9.975 \cdot \text{mA}$   $I_B = \frac{I_C}{\beta} = 0.025 \cdot \text{mA}$ 

Now that's more like it, now  ${\rm I_{\rm B}}$  changes instead of  ${\rm I_{\rm C}}$ .