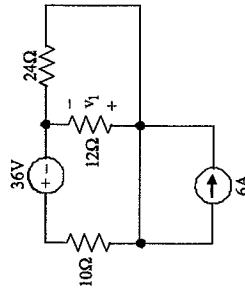


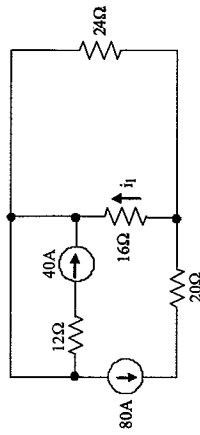
**Problem Session #1 Problems:**

1. Calculate  $v_1$ .



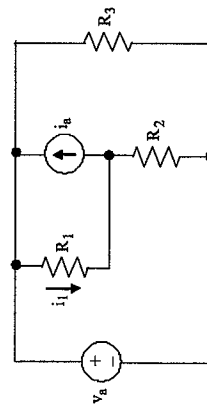
**Solution:**  $v_1 = 16V$

2. Calculate  $i_1$ .



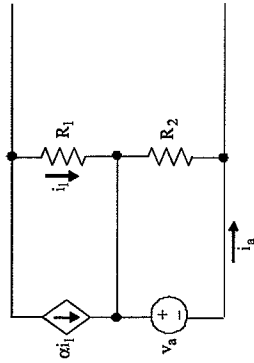
**Solution:**  $i_1 = 48A$

3. Derive an expression for  $i_1$ . The expression must not contain more than the circuit parameters  $v_a$ ,  $i_a$ ,  $R_1$ ,  $R_2$ , and  $R_3$ .



**Solution:**  $i_1 = \frac{v_a}{R_1 + R_2} + i_a \frac{R_2}{R_1 + R_2}$

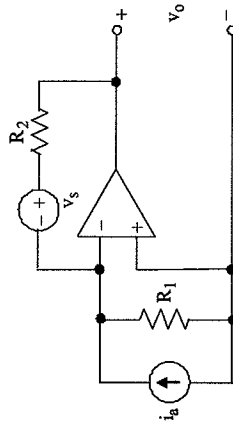
4. Derive an expression for  $i_a$ . The expression must not contain more than the circuit parameters  $\alpha$ ,  $v_a$ ,  $R_1$ , and  $R_2$ .



**Solution:**  $i_a = -\frac{v_a}{R_2} \frac{R_1}{1 + \alpha}$

Make at least one consistency check (other than a units check) on your expression. Explain the consistency check clearly.

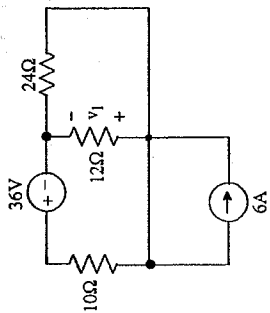
5. The op-amp operates in the linear mode. Using an appropriate model of the op amp, derive an expression for  $v_o$  in terms of not more than  $v_s$ ,  $i_a$ ,  $R_1$ , and  $R_2$ .



**Solution:**  $v_o = v_s - i_a R_2$

1. a. (5 points)

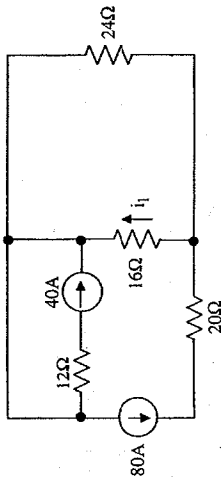
Calculate  $v_1$ .



sol'n: The 6A source across the wire may be ignored. Its current flows through the wire but produces no V-drop. Without the 6A src we have a V-divider:

b. (5 points)  $v_1 = 36V \cdot \frac{12\Omega}{12\Omega + 24\Omega + 10\Omega} = 36V \cdot \frac{8\Omega}{46\Omega} = 16V$

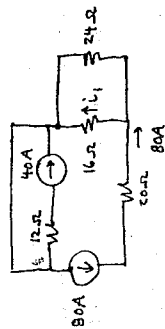
Calculate  $i_1$ .



sol'n: IF we redraw the circuit, we see a current divider:

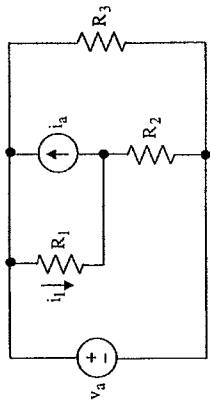
$$i_1 = 80A \cdot \frac{24\Omega}{16 + 24\Omega} = 80A \cdot \frac{24\Omega}{40\Omega}$$

$$i_1 = 48A$$

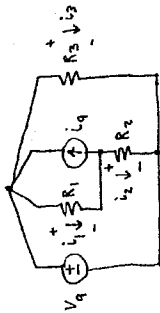


2. (30 points)

Derive an expression for  $i_1$ . The expression must not contain more than the circuit parameters  $v_a$ ,  $i_a$ ,  $R_1$ ,  $R_2$ , and  $R_3$ .



sol'n: Redraw with top as one node:



Current sum at top or bottom node? No, because we would have to define a current for source  $v_a$ .

Current at center node:  $i_a - i_1 + i_2 = 0A$

V-loop around left inner loop:  $v_a - i_1 R_1 - i_2 R_2 = 0V$

No V-loop for other inner loops because we would have to define V-drop for  $i_a$ .

Next larger loop is  $R_1, R_2, R_3$ :  $i_2 R_2 + i_1 R_1 - i_3 R_3 = 0V$

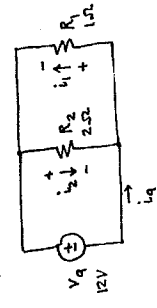
Now we have 3 eqns in 3 unknowns, and we want to find  $i_1$ . We observe, however, that the first two eqns have only two unknowns. So we don't actually need the 3rd eqn. Use 1st eqn to find  $i_2 = i_1 - i_a$ .

Substitute into 2nd eqn:  $v_a - i_1 R_1 - (i_1 - i_a) R_2 = 0V$

$$\text{or } i_1(-R_1 - R_2) = -v_a - i_a R_2 \quad \text{or } i_1 = \frac{v_a + i_a R_2}{R_1 + R_2}$$

soln: 3.b) Many possible answers.

Example: Suppose  $\alpha = 0$ . Choose other simple values:



We see that  $i_q$  is current thru  $R_1 \parallel R_2$  with  $R_1 \parallel R_2$  across  $-V_q$ .

$$R_1 \parallel R_2 = 1 \parallel 2 \Omega = \frac{1 \cdot 2}{1+2} = \frac{2}{3} \Omega$$

$$\therefore i_q = -V_q / R_1 \parallel R_2 = -12V / \frac{2}{3} \Omega = -18A$$

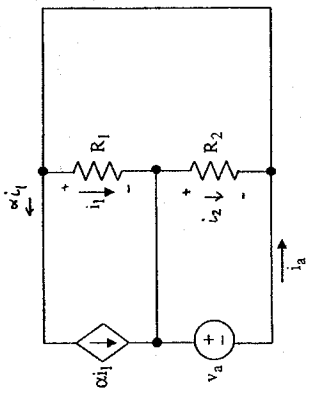
Use formula from (a) with these component

Values:  $i_q = -12V \left( \frac{1}{2\Omega} + \frac{1}{1\Omega} \right) = -12V \cdot \frac{3}{2}$

$i_q = -18V$  ✓ agrees with obvious soln for this simple case

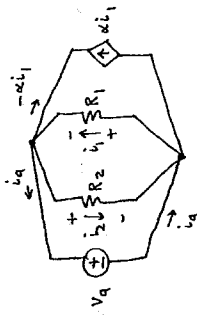
3. (30 points)

a. Derive an expression for  $i_q$ . The expression must not contain more than the circuit parameters  $\alpha$ ,  $V_q$ ,  $R_1$ , and  $R_2$ .



b. Make at least one consistency check (other than a units check) on your expression. Explain the consistency check clearly.

soln: a) Redraw circuit



No current sums at nodes because of  $V_q$ .

V-loop on left:  $V_q - i_2 R_2 = 0V \Rightarrow i_2 = \frac{V_q}{R_2}$

V-loop in middle:  $i_2 R_2 + i_1 R_1 = 0V \Rightarrow i_1 = -\frac{V_q}{R_1}$

We could also just observe that  $V_q$  is across  $R_1$  and  $R_2$ .

Now that we have found  $i_1$  and  $i_2$ , we use a

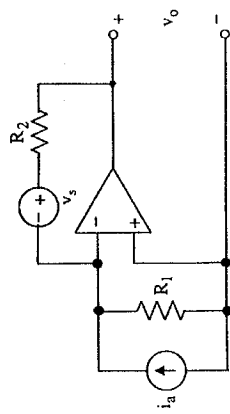
current at top node to find  $i_q$ :

$$i_q + i_2 - i_1 - \alpha i_1 = 0A \text{ or } i_q + \frac{V_q}{R_2} + \frac{V_q}{R_1} + \alpha \frac{V_q}{R_1} =$$

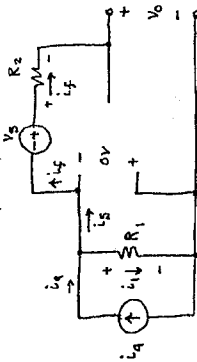
$$\text{or } i_q = -V_q \left( \frac{1}{R_2} + \frac{1}{R_1} + \frac{\alpha}{R_1} \right) \text{ or } i_q = -\frac{V_q}{R_1 \parallel \frac{R_1}{\alpha} \parallel R_2}$$

4. (30 points)

The op-amp operates in the linear mode. Using an appropriate model of the op-amp, derive an expression for  $v_o$  in terms of not more than  $v_s$ ,  $i_a$ ,  $R_1$ , and  $R_2$ .



sol'n: Redrew without op-amp and 0V drop across + and - inputs:



V-loop on left thru  $R_1$  and 0V drop:

$$i_1 R_1 + 0V = 0V \quad \text{or} \quad i_1 = 0$$

Current sum at node above  $R_1$ :

$$-i_4 + i_1 + i_5 = 0A \quad \text{or} \quad i_5 = i_4$$

V-loop on right thru 0V drop,  $v_s$ ,  $R_2$ , and  $v_o$ :

$$-0V + v_s - i_4 R_2 - v_o = 0V \quad \text{or} \quad i_4 = \frac{v_s - v_o}{R_2}$$

Now use  $i_5 = i_4$ .

$$i_a = \frac{v_s - v_o}{R_2} \quad \text{Thus} \quad v_s - v_o = i_a R_2$$

$$v_o = v_s - i_a R_2$$