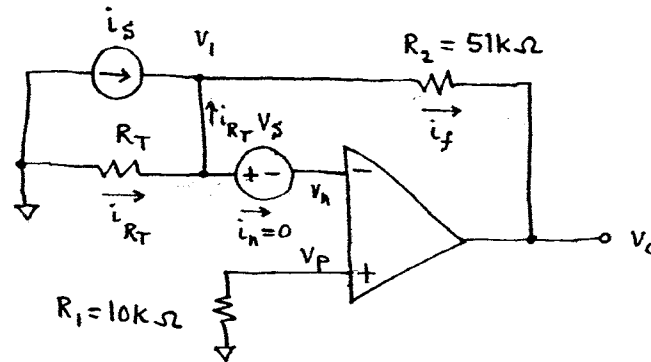


sol'n: 1.a)



- Find  $v_p$ :  $v_p = 0V$  since no current in  $R_1$  so no v-drop for  $R_1$

$$v_n = v_p = 0V$$

- Find  $i_f$  on left side (total current into  $v_1$  node from  $i_s$  and  $R_T$ )

$$v_1 = v_n + v_s = v_s, \text{ and no current flows thru } v_s \text{ since no current flows into op-amp.}$$

$$\therefore i_f \text{ on left side} = i_s + i_{R_T} = i_s + \frac{0 - v_1}{R_T} = i_s + \frac{-v_s}{R_T}$$

- Find  $i_f$  on right side

$$i_f \text{ on right side} = \frac{v_1 - v_o}{R_2} = \frac{v_s - v_o}{R_2}$$

- Set  $i_f$  on left side =  $i_f$  on right side

$$i_s - \frac{v_s}{R_T} = \frac{v_s - v_o}{R_2} \quad \text{or}$$

$$v_o = v_s \left(1 + \frac{R_2}{R_T}\right) - i_s R_2$$

verify: Superposition

$$v_s = 0 \Rightarrow i_{R_T} = 0 \Rightarrow v_o = 0V - i_s R_2 \checkmark$$

$$i_s = 0 \quad i_{R_T} = \frac{-v_s}{R_T} = i_f = \frac{v_s - v_o}{R_2}$$

$$\text{same as having } v_p = v_s \quad v_o = v_s \left(1 + \frac{R_2}{R_T}\right) \checkmark$$

Sol'n: 1. b)

$$R_T(273^\circ\text{K}) = 7250 e^{100^\circ\text{K} \left( \frac{1}{273^\circ\text{K}} - \frac{1}{300^\circ\text{K}} \right)} \Omega \doteq \boxed{7.5 \text{ k}\Omega = R_T(273^\circ)}$$

$$R_T(373^\circ\text{K}) = 7250 e^{100^\circ\text{K} \left( \frac{1}{373^\circ\text{K}} - \frac{1}{300^\circ\text{K}} \right)} \Omega \doteq \boxed{6.8 \text{ k}\Omega = R_T(373^\circ)}$$

c)  $V = v_o(373^\circ\text{K}) - v_o(273^\circ\text{K}) = v_s \left( 1 + \frac{R_2}{R_T(373^\circ)} \right) - v_s \left( 1 + \frac{R_2}{R_T(273^\circ)} \right)$

Note:  $i_s R_2$  terms cancel

$$v_s = \frac{IV}{R_2} \frac{R_T(273^\circ) \cdot R_T(373^\circ)}{R_T(273^\circ) - R_T(373^\circ)} = \frac{1V}{51\text{k}\Omega} \frac{7.5\text{k}\Omega \cdot 6.8\text{k}\Omega}{7.5\text{k}\Omega - 6.8\text{k}\Omega}$$

$$v_s = \frac{1V}{51\text{k}\Omega} \frac{51\text{k}\Omega \cdot \text{k}\Omega^2}{0.7\text{k}\Omega} = \frac{1V}{0.7} = 1.43V \quad \boxed{v_s = 1.43V}$$

d)  $v_o(273^\circ\text{K}) = v_s \left( 1 + \frac{R_2}{R_T(273^\circ)} \right) - i_s R_2 = 0V$

$$i_s = \frac{1V}{0.7} \left( 1 + \frac{51\text{k}\Omega}{7.5\text{k}\Omega} \right) \cdot \frac{1}{51\text{k}\Omega} = \frac{1V}{0.7} \left( \frac{1}{51\text{k}\Omega} + \frac{1}{7.5\text{k}\Omega} \right)$$

$$\boxed{i_s \doteq 218 \mu\text{A} \approx 220 \mu\text{A}}$$

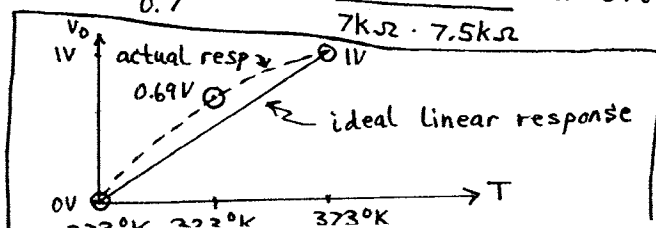
e)  $R_T(323^\circ\text{K}) = 7250 e^{100^\circ\text{K} \left( \frac{1}{323^\circ\text{K}} - \frac{1}{300^\circ\text{K}} \right)} \Omega \doteq 7.08 \text{ k}\Omega \approx 7\text{k}\Omega$

$$v_o(323^\circ) = v_s \left( 1 + \frac{R_2}{R_T(323^\circ)} \right) - i_s R_2 =$$

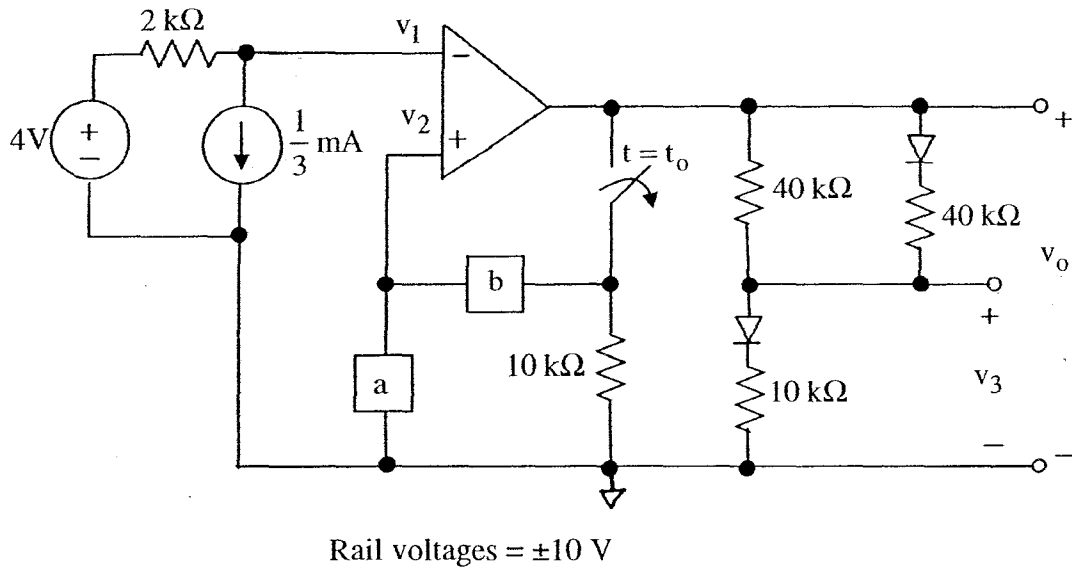
$$= v_s \left( 1 + \frac{R_2}{R_T(273^\circ)} - \frac{R_2}{R_T(273^\circ)} + \frac{R_2}{R_T(323^\circ)} \right) - i_s R_2$$

$$= 0V + v_s R_2 \left( \frac{1}{R_T(323^\circ)} - \frac{1}{R_T(273^\circ)} \right) = \frac{1V}{0.7} 51\text{k}\Omega \left( \frac{1}{7\text{k}\Omega} - \frac{1}{7.5\text{k}\Omega} \right)$$

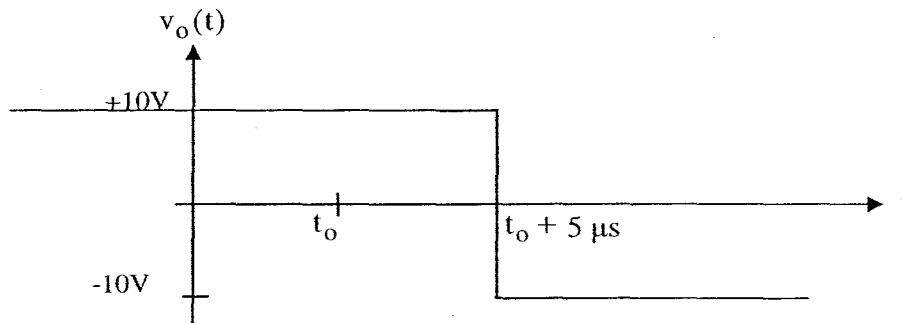
$$= \frac{1V}{0.7} 51\text{k}\Omega \frac{7.5\text{k}\Omega - 7\text{k}\Omega}{7\text{k}\Omega \cdot 7.5\text{k}\Omega} \doteq 0.69V$$



2.



After being closed for a long time, the switch closes at  $t = t_0$ .



- Choose either an R or L to go in box a and either an R or L to go in box b to produce the  $v_o(t)$  shown above. Specify which element goes in each box and its value.
- Sketch  $v_1(t)$ , showing numerical values appropriately.
- Sketch  $v_2(t)$ , showing numerical values appropriately.
- Sketch  $v_3(t)$ . Show numerical values for  $t < t_0$ , for  $t_0 < t < t_0 + 5 \mu s$ , and for  $t_0 + 5 \mu s < t$ . Use the ideal model of the diode: when forward biased, its resistance is zero; when reverse biased, its resistance is infinite.

Explain your work carefully.

# HW #10 Cont.

ECE 1000

Su 05

Sol'n: 2.a) Consider possibilities.

$a=R$  and  $b=R$

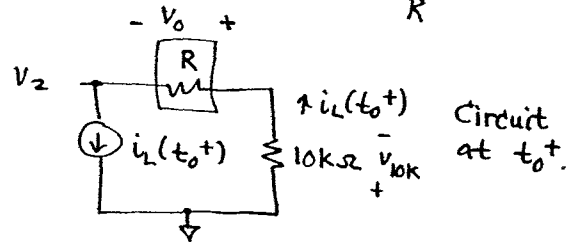
Doesn't work.  $v_2$  would change at  $t_0$  but never again. Delay of  $5\mu s$  not possible.

$a=L$  and  $b=L$

Doesn't work. Before time  $t_0$ , the  $L$ 's look like wires and would short  $v_0$  to ref. But  $v_0 = \pm v_{Rail} = \pm 10V$ . Thus, we would have an invalid circuit.

$a=L$  and  $b=R$

Before  $t_0$ , the  $L$  looks like a wire, and  $v_2 = 0V$ .  $i_L(t_0^-) = \frac{v_0}{R} = i_L(t_0^+)$ .



At  $t_0^+$ , the current in  $R$  will be  $i_L(t_0^+) = i_L(t_0^-) = \frac{v_0}{R}$  or the same as at  $t_0^-$ . Thus, the  $v$ -drop for  $R$  at  $t_0^+$  will be  $v_0$ . Current  $i_L(t_0^+)$  flowing in the  $10k\Omega$  will cause a voltage drop in series with the drop for  $R$ , resulting in a very negative voltage at  $v_2$ . This would cause  $v_0$  to go low at  $t = t_0^+$  rather than after a delay of  $5\mu s$ .

$\therefore$  This case doesn't work.

# HW #10 Cont.

ECE 1000

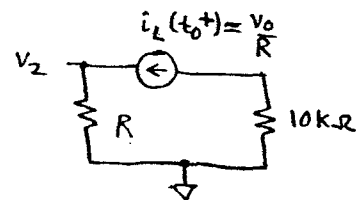
Su 05

Sol'n: 2.a) cont.

$$a = R \text{ and } b = L$$

$$i_L(t_0^-) = \frac{V_0}{R} \text{ as in prev case.}$$

At  $t_0^+$  with  $i_L(t_0^+) = i_L(t_0^-) = \frac{V_0}{R}$ :



$$\text{We have } v_2(t_0^+) = \frac{V_0}{R} \cdot R = V_0.$$

$\underbrace{\hspace{1.5cm}}_{i_L(t_0^+)}$

So  $v_2$  doesn't change immediately.

This will work!

For  $t \rightarrow \infty$  we will have  $v_2 = 0V$

since there is no power source.

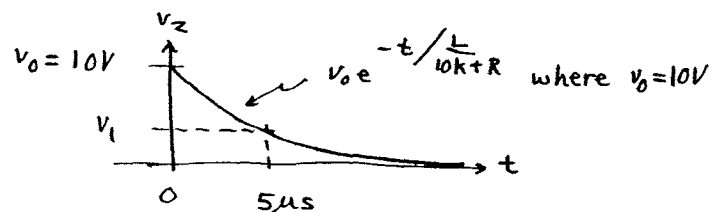
Using the general formula for

$v_2(t)$ , we have:

$$v_2(t) = \underbrace{v_2(t \rightarrow \infty)}_{0V} + \underbrace{[v_2(t_0^+) - v_2(t \rightarrow \infty)]}_{V_0} e^{-\frac{t}{R_{Th}}} \underbrace{e^{-\frac{t}{R_{Th}}}}_{0V}$$

where  $R_{Th} = 10k\Omega + R$

$$v_2(t) = V_0 e^{-\frac{t}{10k+R}}$$



The output,  $v_0$ , will drop at

$t_0 + 5\mu s$  if  $v_2(t_0 + 5\mu s) = v_1$ .

[Assume  $t_0 = 0$  for convenience.]

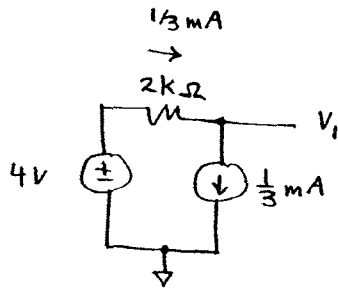
Now find  $v_1$ .

# HW #10 Cont.

ECE 1000

Su 05

sol'n: 2.a) cont.



$$V_1 = 4V - \frac{1}{3} \text{ mA} \cdot 2 \text{ k}\Omega$$

$$V_1 = 4V - \frac{2}{3} \text{ V} = \frac{10}{3} \text{ V}$$

$$\therefore \text{ we want } v_2(5\mu\text{s}) = V_1 = \frac{10}{3} \text{ V}$$

$$\text{or } 10 \text{ V } e^{-5\mu\text{s}/\frac{L}{10\text{k}\Omega + R}} = \frac{10}{3} \text{ V}$$

$$-5\mu\text{s}/\frac{L}{10\text{k}\Omega + R} = \ln \frac{1}{3} \doteq -1.1$$

$$\text{or } 5\mu\text{s} = 1.1 \frac{L}{10\text{k}\Omega + R}$$

If we use  $R = 12\text{k}\Omega$  we get a convenient value for  $L$ . Many solutions for  $R$  and  $L$  will work, however.

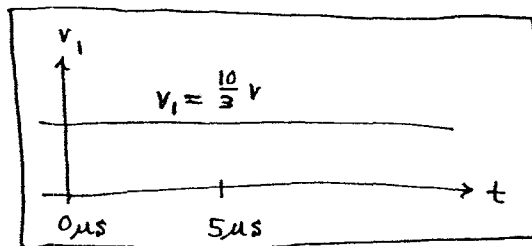
$$R = 12\text{k}\Omega \text{ gives } L = \frac{5\mu\text{s} \cdot (10\text{k}\Omega + 12\text{k}\Omega)}{1.1}$$

$$L = 5\mu\text{s} \cdot 20\text{k}\Omega = 100 \text{ mH}$$

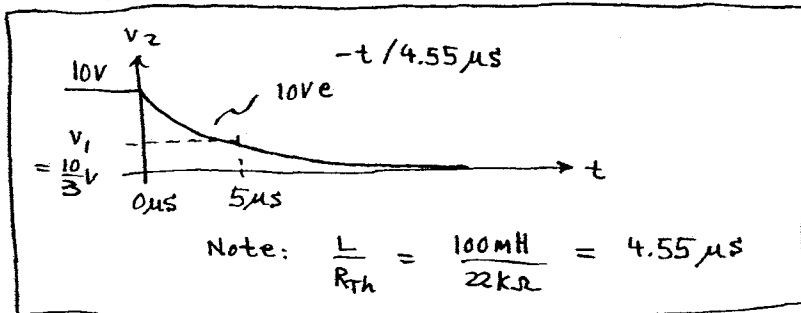
$R = 12\text{k}\Omega \quad L = 100 \text{ mH}$

one solution among many.

b)



c)

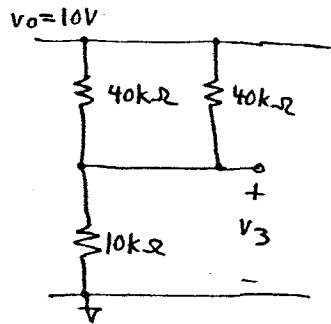


# HW #10 Cont.

ECE 1000

Su 05

sol'n: 2.d) For  $v_o = +10V$ , both diodes are forward biased and look like wires.

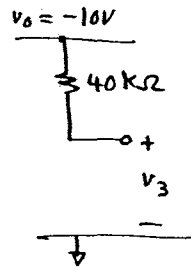


$$v_3 = 10V \cdot \frac{10k\Omega}{10k\Omega + 40k\Omega \parallel 40k\Omega}$$

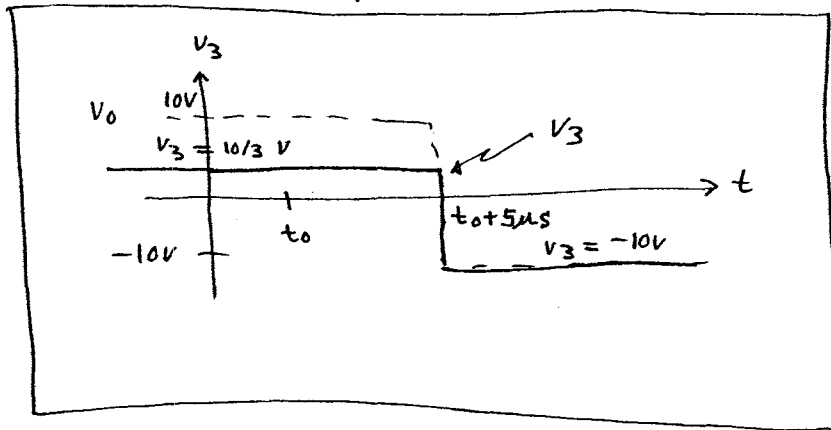
$$= 10V \cdot \frac{10k\Omega}{10k\Omega + 20k\Omega}$$

$$v_3 = \frac{10}{3} V$$

For  $v_o = -10V$ , both diodes are reverse biased and look like open circuits.

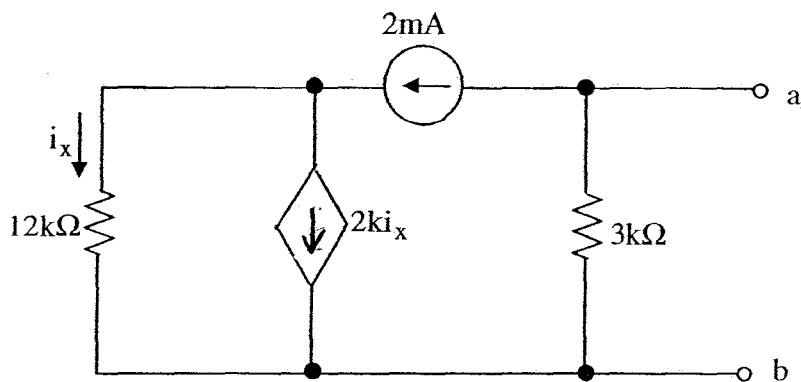


$$v_3 = -10V$$



HW #10 Cont.

3.



- Find the Thevenin equivalent of the above circuit relative to terminals a and b.
- If we attach  $R_L$  to terminals a and b, find the value of  $R_L$  that will absorb maximum power.
- Calculate the value of that maximum power absorbed by  $R_L$ .



# HW#10 Cont.

ECE 1000

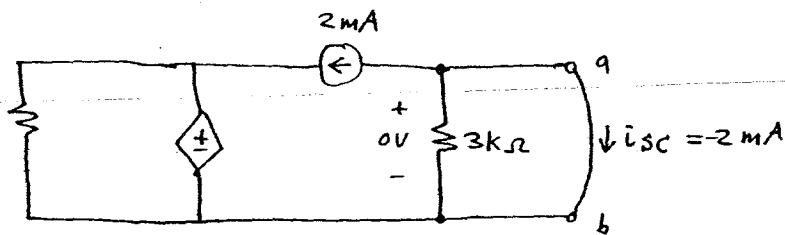
Su 05

sol'n: 3. a)  $V_{Th} = V_{a,b} \text{ open circ} = -2 \text{ mA} \cdot 3 \text{ k}\Omega = -6 \text{ V}$

The current source is between a,b and the  $12 \text{ k}\Omega$  and dependent source.

The current source thus isolates behavior at a,b from the  $12 \text{ k}\Omega$  and dependent source.

Use  $i_{sc}$  to find  $R_{Th}$ :



we short a,b so no v-drop across  $3 \text{ k}\Omega$ .

So  $i_{3 \text{ k}\Omega} = 0$  and  $i_{sc} = -2 \text{ mA}$ .

$$R_{Th} = \frac{V_{Th}}{i_s} = \frac{-6 \text{ V}}{-2 \text{ mA}} = 3 \text{ k}\Omega$$

$V_{Th} = -6 \text{ V} \quad R_{Th} = 3 \text{ k}\Omega$

Comments: 1) We could also just turn off the  $2 \text{ mA}$  source and look into a,b to see  $R_{Th} = 3 \text{ k}\Omega$ .

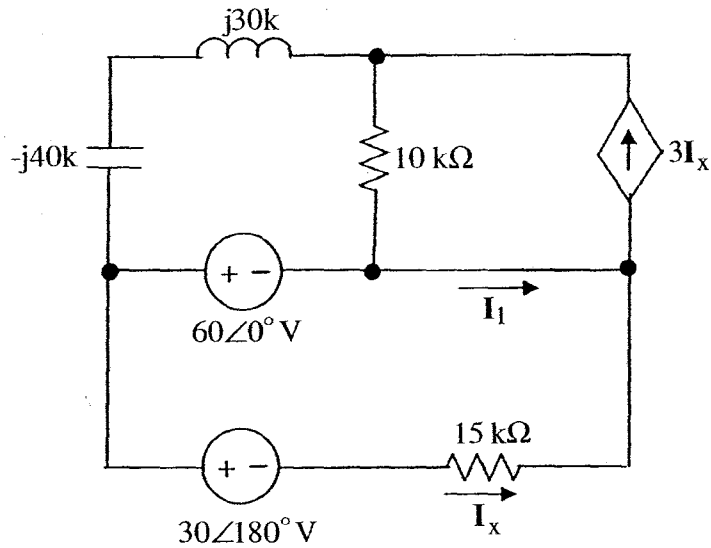
2) we really just started with a Norton equivalent that we converted to Thevenin equivalent.

b) max pwr when  $R_L = R_{Th} = 3 \text{ k}\Omega = R_L$

c) max pwr  $P_{max} = \frac{V_{Th}^2}{4 R_{Th}} = \frac{(-6 \text{ V})^2}{4 \cdot 3 \text{ k}\Omega} = 3 \text{ mW} = P_{max}$

HW #10 Cont.

4.



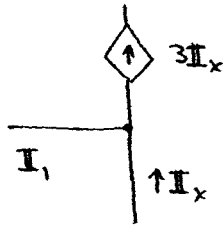
- A frequency-domain circuit is shown above. Write the value of phasor  $I_1$  in polar form.
- Given  $\omega = 53.13$  rad/s, write a numerical time-domain expression for  $i_1(t)$ , the inverse phasor of  $I_1$ .

# HW #10 Cont.

Su 05

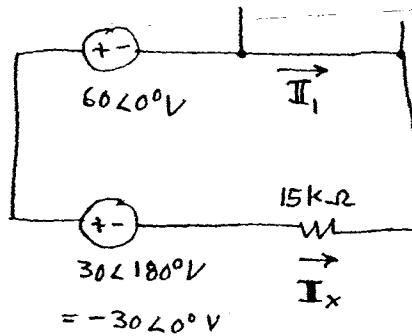
ECE 1000

sol'n: 4. a) Sum of currents for node on right side:



We see that  $I_1 = 2I_x$   
from sum of currents  
out of node = 0.

From the bottom half of the circuit, we  
can compute  $I_x$  directly:



From v-loop we have

$$I_x = \frac{60\angle 0^\circ\text{V} - 30\angle 0^\circ\text{V}}{15\text{k}\Omega}$$

$$I_x = \frac{30\angle 0^\circ\text{V}}{15\text{k}\Omega}$$

$$I_x = 6\text{ mA } \angle 0^\circ$$

$$\text{So } I_1 = 2I_x = 12\text{ mA } \angle 0^\circ$$

$$I_1 = 12\angle 0^\circ\text{ mA}$$

b)

$$i_1(t) = 12 \cos(53.13t)\text{ mA}$$

or  $\pi t$