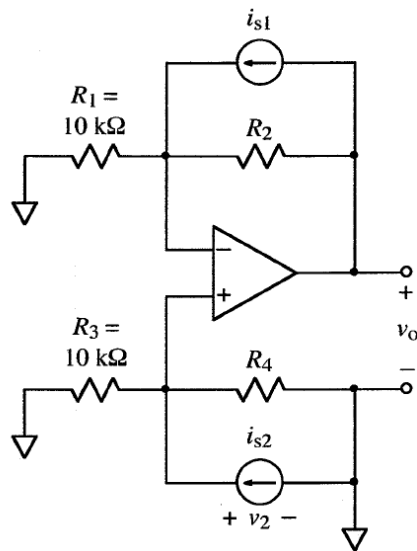


1.



The above circuit operates in linear mode. Derive a symbolic expression for v_o . The expression must contain not more than the parameters i_{s1} , i_{s2} , R_1 , R_2 , R_3 , and R_4 .

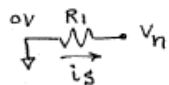
sol'n: a) First, we calculate v_p . No current flows into the op-amp, leaving a current divider. Equivalently, we have R_3 in parallel with R_4 driven by current source i_{s2} .

$$v_p = i_{s2} \cdot R_3 \parallel R_4$$

Since the op-amp is operating in linear mode, $v_n = v_p$.

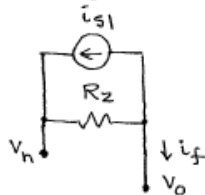
$$v_n = v_p = i_{s2} \cdot R_3 \parallel R_4$$

Now we the current flowing toward the - input from the left



$$i_3 = \frac{0V - v_n}{R_1} = -\frac{v_n}{R_1}$$

Since no current flows into the op-amp, we have the same current flowing in the feedback. We calculate the feedback current, i_f , using v_n .



$$i_f = -i_{s1} + \frac{v_n - v_o}{R_2}$$

We set $i_s = i_f$ and solve for v_o .

$$-\frac{v_n}{R_1} = -i_{s1} + \frac{v_n - v_o}{R_2}$$

or

$$\frac{v_o}{R_2} = -i_{s1} + \frac{v_n}{R_2} + \frac{v_n}{R_1}$$

or

$$v_o = -i_{s1} R_2 + v_n \left(1 + \frac{R_2}{R_1} \right)$$

or

$$v_o = -i_{s1} R_2 + i_{s2} R_3 \parallel R_4 \cdot \left(1 + \frac{R_2}{R_1} \right)$$

2.

If $i_{s1} = 10 \mu\text{A}$ and $i_{s2} = 0 \mu\text{A}$, find the value of $R_2 = R_4$ that will yield an output voltage of $v_o = 1 \text{ V}$.

If $i_{s2} = 0 \mu\text{A}$, then $v_p = 0 \text{ V}$ and $v_n = v_p = 0 \text{ V}$. It follows that all of i_{s1} must flow thru R_2 .

Thus,

$$v_o = -i_{s1} R_2$$

or

$$R_2 = \frac{v_o}{-i_{s1}} = \frac{1 \text{ V}}{-10 \mu\text{A}}$$

or

$$R_2 = -100 \text{ k}\Omega$$

3.

Write a formula for the circuit's input resistance, R_{in} , as seen by source i_{s2} . In other words, write a formula for voltage, v_2 , across i_{s2} divided by i_{s2} :

$$R_{in} = \frac{v_2}{i_{s2}}$$

Write R_{in} in terms of not more (and possibly less) than R_1 , R_2 , R_3 , and R_4 .

v_2 is the voltage across i_{s2} , as shown in the diagram. $v_2 = v_p$, (the voltage at the + input).

$$v_2 = i_{s2} \cdot R_3 \parallel R_4 \quad (\text{see answer to part (a)})$$

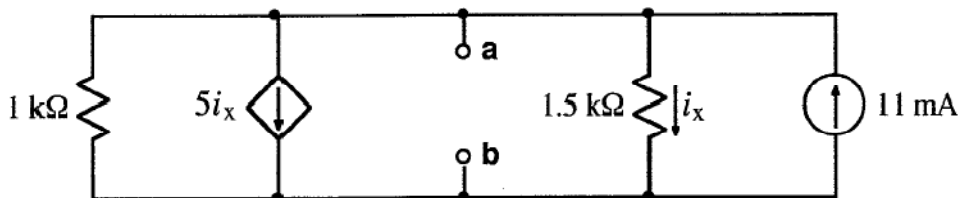
Using this result, we find R_{in} :

$$R_{in} = \frac{v_2}{i_{s2}} = \frac{i_{s2} R_3 \parallel R_4}{i_{s2}}$$

or

$$R_{in} = R_3 \parallel R_4$$

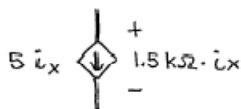
4.



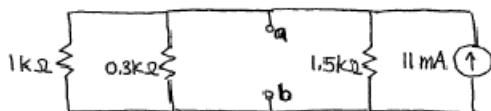
Find the Thevenin equivalent of the above circuit relative to terminals a and b.

We observe that the voltage across all the components is the same, and it is equal to $i_x \cdot 1.5 \text{ k}\Omega$.

For the dependent source, we may find an equivalent resistance:



$$R_{eq} = \frac{v}{i} = \frac{1.5 \text{ k}\Omega \cdot i_x}{5 i_x} = 0.3 \text{ k}\Omega$$



The V_{Th} is the voltage across a, b and is equal to the 11 mA current times the combined parallel impedance.

$$V_{Th} = 11 \text{ mA} \cdot 1 \text{ k}\Omega \parallel 1.5 \text{ k}\Omega \parallel 0.3 \text{ k}\Omega$$

$$\text{we have } 1.5 \text{ k}\Omega \parallel 0.3 \text{ k}\Omega = 0.3 \text{ k}\Omega \cdot \frac{5}{6}$$

$$= 0.3 \text{ k}\Omega \cdot \frac{5}{6}$$

$$= 250 \Omega$$

$$\text{and } 1 \text{ k}\Omega \parallel 250 \Omega = 250 \Omega \cdot \frac{4}{5}$$

$$= 250 \Omega \cdot \frac{4}{5}$$

$$= 200 \Omega$$

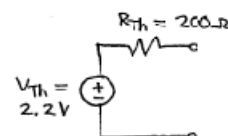
$$V_{Th} = 11 \text{ mA} \cdot 200 \Omega = 2.2 \text{ V}$$

To find R_{Th} , we turn off the independent 11 mA source and look into a, b. We have

$$R_{Th} = 1 \text{ k}\Omega \parallel 1.5 \text{ k}\Omega \parallel 0.3 \text{ k}\Omega$$

$$\text{or } R_{Th} = 200 \Omega$$

Thevenin equivalent:



5. a)

If we attach R_L to terminals **a** and **b**, find the value of R_L that will absorb maximum power.

b)

Calculate the value of that maximum power absorbed by R_L .

For max pwr transfer, we use

$$R_L = R_{Th} = 200\ \Omega.$$

When $R_L = R_{Th}$, we achieve the max pwr transfer:

$$P_{max} = \frac{V_{Th}^2}{4 R_{Th}}$$

$$= \frac{(2.2V)^2}{4(200\ \Omega)}$$

$$P_{max} = 6.05\ \text{mW}$$