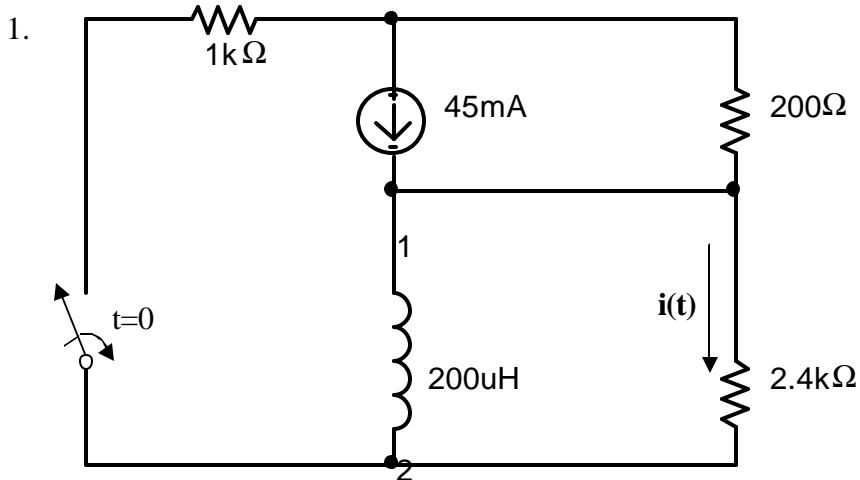


UNIVERSITY OF UTAH
ELECTRICAL AND COMPUTER ENGINEERING DEPARTMENT

ECE 1270

HOMEWORK #6 Solution

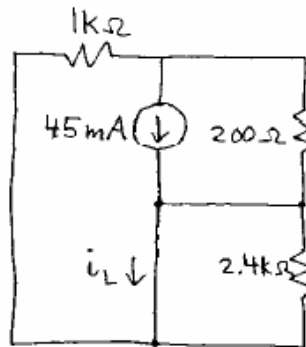
Summer 2007



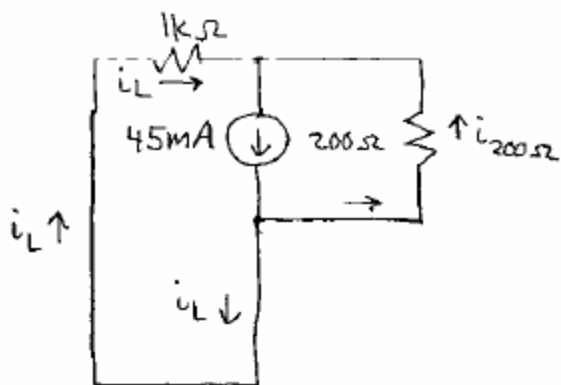
After being open for a long time, the switch closes at $t=0$.

- a) Calculate the energy stored on the inductor as $t \rightarrow \infty$.
- b) Write a numerical expression for $i(t)$ for $t > 0$.

sol'n: a) As $t \rightarrow \infty$, the L acts like a wire.



Since the $2.4\text{k}\Omega$ is shorted out by wires, we may ignore it. This leaves a current divider formed by the $1\text{k}\Omega$ and 200Ω resistors for current from the 45mA source.



$$i_L = 45\text{mA} \cdot \frac{200\Omega}{200\Omega + 1\text{k}\Omega} = 45\text{mA} \cdot \frac{1}{6}$$

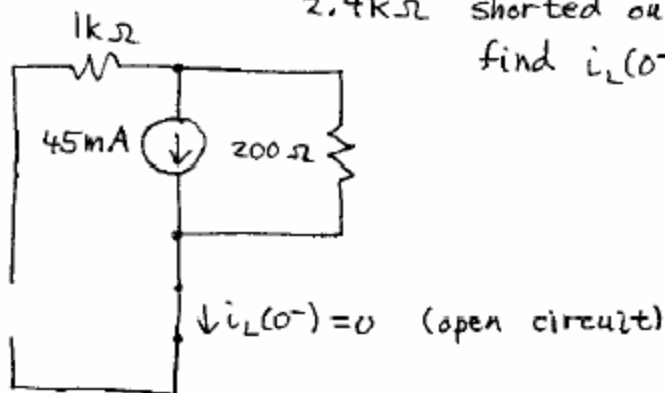
$$i_L = 7.5\text{mA}$$

For an inductor, $w_L = \frac{1}{2} L i_L^2$:

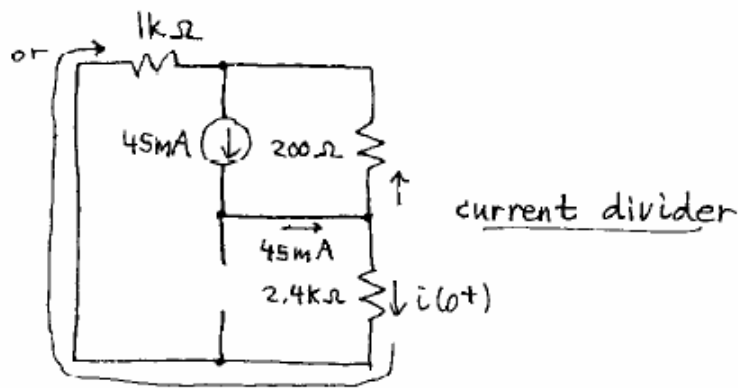
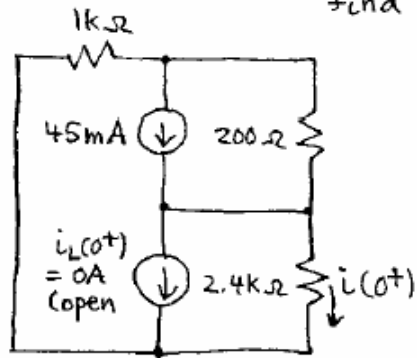
$$\begin{aligned} w_L(t \rightarrow \infty) &= \frac{1}{2} \cdot 200\mu\text{H} \cdot (7.5\text{mA})^2 \\ &= 100\mu\text{H} \cdot \left(\frac{3}{4}\right)^2 (10\text{mA})^2 \\ &= \frac{9}{16} \cdot 100\mu \cdot 100\mu \text{J} \\ &= \frac{9}{16} \cdot 10\text{k} \mu\mu\text{J} \\ &= \frac{90}{16} \text{ nJ} \end{aligned}$$

$$w_L(t \rightarrow \infty) = 5.625 \text{ nJ}$$

- b) $t = 0^-$ model: $L = \text{wire}$, switch open
 $2.4\text{k}\Omega$ shorted out (so ignore)
 find $i_L(0^-)$



$t=0^+$ model: $L =$ current source: $i_L(0^+) = i_L(0^-)$
 find $i(0^+)$ (switch closed)



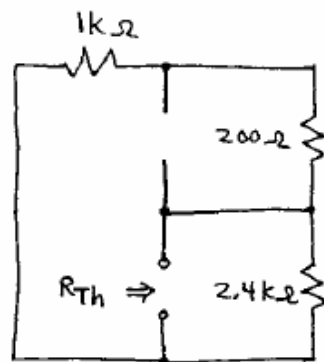
we have a current divider:

$$i(0^+) = 45\text{mA} \cdot \frac{200\Omega}{1\text{k}\Omega + 2.4\text{k}\Omega + 200\Omega} = \frac{45\text{mA}}{12}$$

$$\text{or } i(0^+) = \frac{15}{4} \text{ mA}$$

From part (a) we know $i(t \rightarrow \infty) = 0$
 since the $2.4\text{k}\Omega$ is shorted by the
 L and the wire on the middle right
 side.

$\tau = \frac{L}{R_{TH}}$ where R_{TH} = Thevenin R for terminals where L is connected.



We turn off the independent source and look into the terminals where L is connected.

$$R_{TH} = 2.4k\Omega \parallel (1k\Omega + 200\Omega)$$

$$= 2.4k\Omega \parallel 1.2k\Omega$$

$$= 1.2k\Omega \cdot \frac{2}{2+1} = 1.2k\Omega \cdot \frac{2}{3}$$

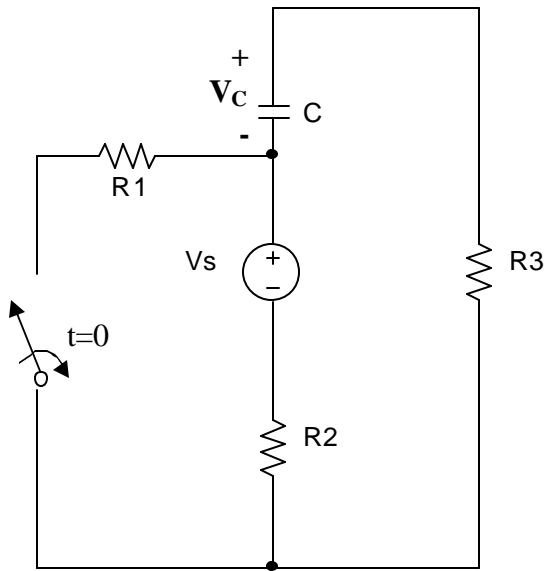
$$R_{TH} = 800\Omega \quad \tau = \frac{200\mu H}{800\Omega} = \frac{1}{4}\mu s$$

$$\text{or } \tau = 250\text{ ns}$$

$$\text{Use } i(t) = i(t \rightarrow \infty) + [i(0^+) - i(t \rightarrow \infty)] e^{-t/\tau} \quad t > 0$$

$$\therefore i(t) = 0 + \left[\frac{15}{4} \text{ mA} - 0 \right] e^{-t/250\text{ ns}} = 3.75 \text{ mA} e^{-t/250\text{ ns}} \quad \text{for } t > 0$$

2.



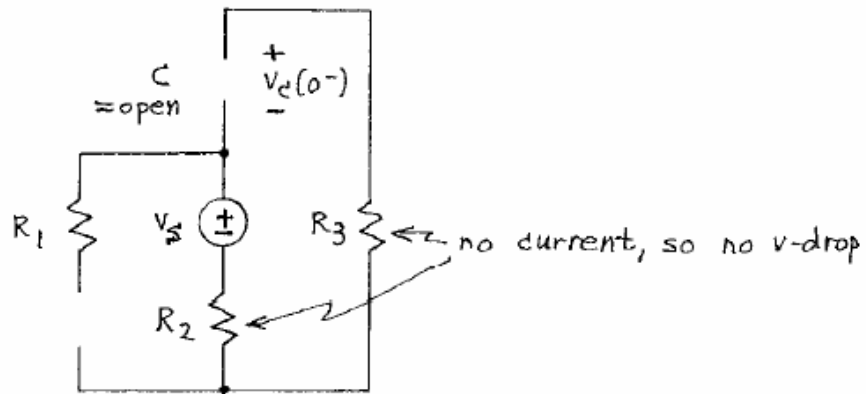
After being open for a long time, the switch becomes closed at $t=0$.

a) Write an expression for $V_c(t=0^+)$.

b) Write an expression for $V_c(t>0)$ in terms of $R1$, $R2$, $R3$, V_s , and C .

sol'n: a) We use $v_c(t=0^+) = v_c(0^-)$.

$t=0^-$ model: C acts like open circuit
switch is open



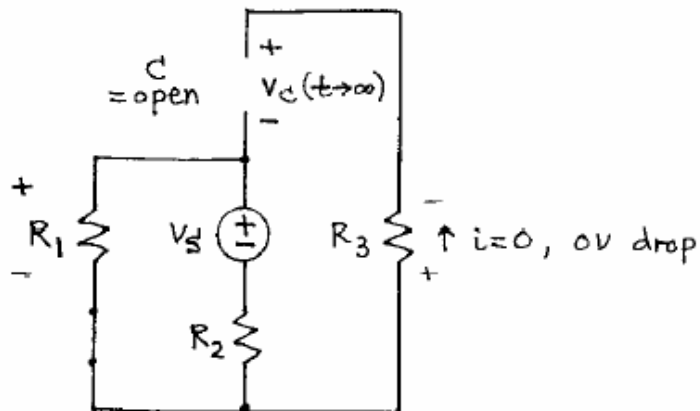
No current flows. $v_c(0^+) = v_c(0^-) = -V_s$

b) We use the general form of sol'n:

$$v_c(t > 0) = v_c(t \rightarrow \infty) + [v_c(0^+) - v_c(t \rightarrow \infty)] e^{-t/\tau}$$

where $\tau = R_{TH} C$ (using Thevenin equiv where C connected)

$t \rightarrow \infty$ model: $C = \text{open}$, switch closed

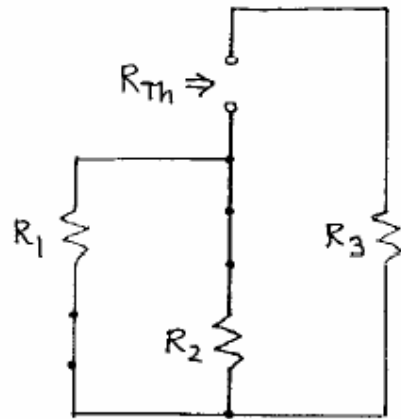


Since there is no v -drop across R_3 , we have $v_c(t \rightarrow \infty) = -v$ -drop across R_1 from v -loop around outside of circuit.

$$v\text{-drop across } R_1 = v_S \frac{R_1}{R_1 + R_2} \quad (v\text{-divider})$$

$$\therefore v_c(t \rightarrow \infty) = -v_S \frac{R_1}{R_1 + R_2}$$

$\tau = R_{TH} C$: We remove C and turn off v_S . Then we look into circuit from terminals where C connected.



We have $R_{Th} = R_1 \parallel R_2 \parallel R_3$

Combining results, we have our solution:

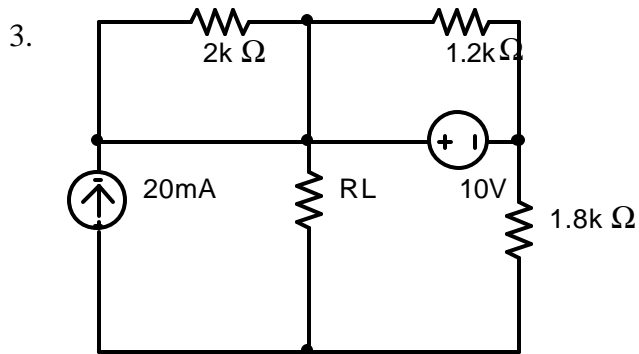
$$v_c(t > 0) = -V_s \frac{R_1}{R_1 + R_2} + \left[-V_s + V_s \frac{R_1}{R_1 + R_2} \right] e^{-t / (R_1 \parallel R_2 + R_3) C}$$

or

$$v_c(t > 0) = -V_s \left\{ \frac{R_1}{R_1 + R_2} + \frac{R_2}{R_1 + R_2} e^{-t / (R_1 \parallel R_2 + R_3) C} \right\}$$

or

$$v_c(t > 0) = -V_s + V_s \frac{R_2}{R_1 \parallel R_2} \left[1 - e^{-t / (R_1 \parallel R_2 + R_3) C} \right]$$



a) Calculate the value of R_L that would absorb maximum power.

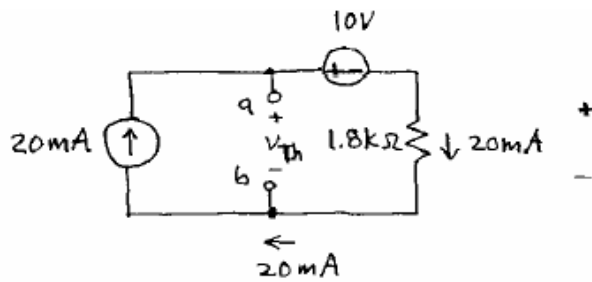
b) Calculate that value of maximum power R_L could absorb.

sol'n: $R_L = R_{Th}$ for max power transfer where the Thevenin equivalent is with respect to terminals a and b (without R_L).

We observe that the $2k\Omega$ resistor on top is shorted out by wires and may be ignored.

We also observe that the $1.2k\Omega$ resistor on top is directly across the $10V$ source and may be treated as a separate circuit having no effect on the rest of the circuit other than to draw some current from the $10V$ source.

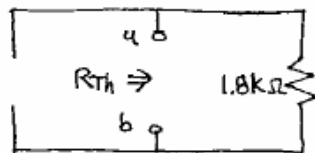
That leaves us with the following circuit:



V_{Th} = voltage across a, b terminals with no load from a to b.

We have $v_{ab} = 20mA \cdot 1.8k\Omega + 10V = 46V$

To find R_{Th} , we turn off the two independent sources and look into the circuit from the a and b terminals:



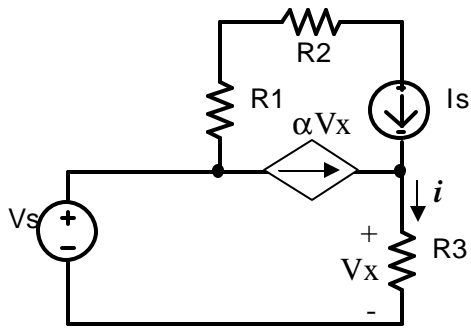
We see $1.8k\Omega$ across a and b.

$$R_{Th} = 1.8k\Omega$$

$$\therefore R_L = 1.8k\Omega$$

$$b) \quad \max \text{ pwr} = \frac{V_{Th}^2}{4R_{Th}} = \frac{(46V)^2}{4 \cdot 1.8k\Omega} \doteq 293.9 \text{ mW}$$

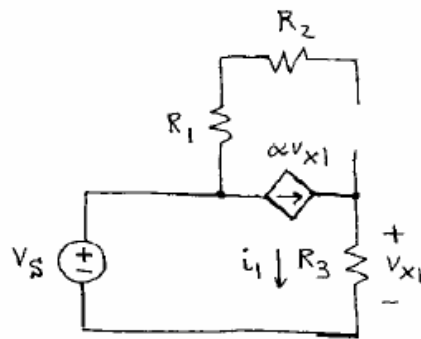
4.



Using superposition, derive an expression for i that contains no circuit quantities other than I_s , V_s , R_1 , R_2 , R_3 , and α , where $\alpha > 0$.

sol'n: We turn on one independent source at a time, find i for each source, and sum the i 's.

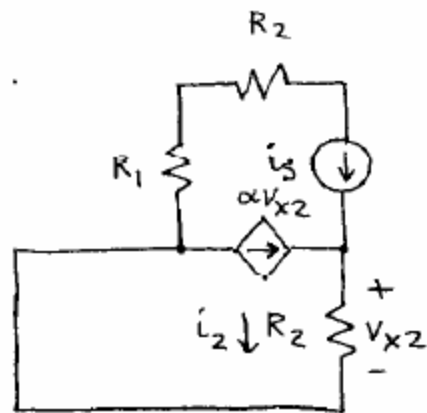
case I: v_s on and i_s off (= open)



$$\text{We have } i_1 = \alpha V_{x1} = \frac{V_{x1}}{R_3}$$

Unless $\alpha = \frac{1}{R_3}$ exactly, (which is impossible in practice), we must have $V_x = 0$, $i_1 = 0$.

case II: v_s off, i_s on
(=wire)



We have the following current summation at the node on the right side:

$$-i_s - \alpha i_2 R_2 + i_2 = 0$$

or

$$i_2 (1 - \alpha R_2) = i_s$$

or

$$i_2 = \frac{i_s}{1 - \alpha R_2}$$

Now we sum the i_1 and i_2 :

$$i = i_1 + i_2 = 0 + \frac{i_s}{1 - \alpha R_2}$$

$$i = \frac{i_s}{1 - \alpha R_2}$$