

## ECE 6180 Stepped-Impedance Filter Design

Portfolio Question: How do you design a stepped-impedance filter?

Text Section 8.6

What is a stepped impedance filter?

- Made up of high impedance (thin) and low impedance (thick) lines
  - Want  $Z_{\text{high}} / Z_{\text{low}}$  to be as large as possible, so this is determined by manufacturing.
  - In our case,  $Z_{\text{high}} = 100$  ohms, and  $Z_{\text{low}} = 10$  ohms.
- Impedances stay the same, but lengths change for each section. Each length is less than  $\lambda/4$ .

Why a stepped impedance filter?

- Smaller than stub-filter
- Easier to design (no Kuroda identities!)

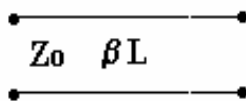
Why NOT a stepped impedance filter?

- Approximations in the design equations make them less accurate

Analysis of stepped impedance filters:

(Note: these are analysis steps, not design steps. You don't do these each time you design a filter, they are just to show how the stepped impedance filter is derived.)

1. For a length of transmission line: (see table p.208)



$$A = \cos(\beta\ell)$$

$$B = jZ_0 \sin(\beta\ell)$$

$$C = jY_0 \sin(\beta\ell)$$

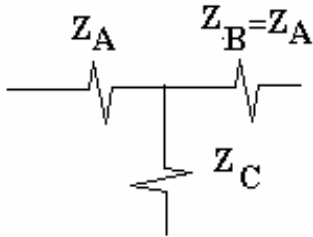
$$D = \cos(\beta\ell)$$

2. Convert from ABCD to Z-matrix (table p. 211)

$$Z_{11} = Z_{22} = \frac{A}{C} = -jZ_0 \cot \beta \ell$$

$$Z_{12} = Z_{21} = \frac{1}{C} = -jZ_0 \csc \beta \ell$$

3. Calculate the Z-matrix of a T-junction circuit (p.195)



$$Z_{11} = Z_{22} = Z_A + Z_C$$

$$Z_{12} = Z_{21} = Z_C$$

4. Relate  $Z_A$ ,  $Z_C$  to  $Z_{11}$ , etc. (Solve for  $Z_{11}$ , etc.)

$$Z_A = Z_{11} - Z_{12} = -jZ_0 \left[ \frac{\cos \beta \ell - 1}{\sin \beta \ell} \right] = jZ_0 \tan \left( \frac{\beta \ell}{2} \right)$$

$$Z_C = Z_{12} = -jZ_0 \csc \beta \ell$$

4. Are  $Z_A$  and  $Z_C$  inductors or capacitors?

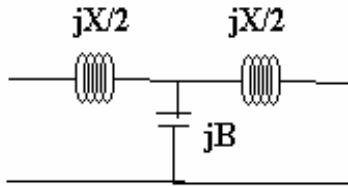
For a length of line with  $\beta L < \lambda/2$  :

$Z_A = +$  imaginary part (inductor)

$Z_C = -$  imaginary part (capacitor)

$$Z_A = j \frac{X}{2} = -jZ_0 \left[ \frac{\cos \beta \ell - 1}{\sin \beta \ell} \right] = jZ_0 \tan \left( \frac{\beta \ell}{2} \right) \Rightarrow X = 2Z_0 \tan \left( \frac{\beta \ell}{2} \right)$$

$$Z_C = \frac{1}{jB} = -jZ_0 \csc \beta \ell \Rightarrow B = \frac{1}{Z_0 \csc \beta \ell} = \frac{1}{Z_0} \sin \beta \ell$$



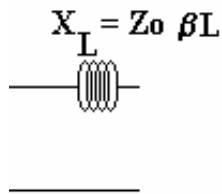
5. Assume a short length of line ( $\beta < \lambda/4$ ) ....

(Here are the approximations that make this method less than perfectly accurate...)

a. When  $Z_0$  is large:

$$X \approx 2Z_0 \left( \frac{\beta \ell}{2} \right) = Z_0 \beta \ell$$

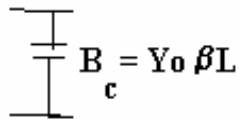
$$B \approx 0$$



b. When  $Z_0$  is small:

$$X \approx 0$$

$$B \approx \frac{1}{Z_0} \beta \ell$$



6. Solve for lengths of lines that are needed for filter design:

$$\beta\ell = \frac{LZ_o}{Z_{high}}$$

$$\beta\ell = \frac{CZ_{low}}{Z_o}$$

Note: These lengths are given in RADIANS. HP/Eesof ADS Linecalc (e\_eff) is given in DEGREES. Multiply these values by  $180 / \pi$  to get them in degrees.

### **Filter Design Steps:**

1. Design the lumped element filter as before (sections 8.3 and 8.4)
2. Solve for lengths ( $\beta L$ ) of each element. (Remember to convert to degrees if using Linecalc.)